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## Polyethylene passive samplers to determine sediment–pore water distribution coefficients of persistent organic pollutants in five heavily contaminated dredged sediments

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### Abstract :

Pore concentration and partition coefficients of polycyclic aromatic hydrocarbons (PAHs) and polychlorinated biphenyls (PCBs) were determined in sediments from five distinct contaminated sites in France (marine harbour, rivers canals and highway sedimentation tank). The assessment of the risk caused by such micropollutants requires, in most cases, the measurement of their availability. To assess this availability, low density polyethylene (LDPE) membrane samplers were exposed to these sediments under constant and low-level agitation over a period of 46 days. Freely dissolved pore water contaminant concentrations were estimated from the concentration at equilibrium in the LDPE membrane. The depletion of contaminants in the sediments was monitored by the use of performance reference compounds (PRCs). Marked differences in freely dissolved PAH and PCB concentrations and resulting sediment–pore water partition coefficients between these five sediments were observed. Data set was tested onto different empirical and mechanistic models. As final findings, triple domain sorption (a total organic carbon, black carbon and oil phase model) could model PCB data successfully whereas the best fitting for PAH partitioning was obtained by Raoult's Law model.

### Highlights

► Hydrophobic organic compounds were determined in pore water in dredged sediments. ► Freely dissolved pore water concentrations were estimated by passive sampler. ► Sediment depletion was evaluated with performance reference compounds. ► Distribution coefficients were well predicted with empirical and mechanistic models.

**Keywords :** Passive sampling, Pore water concentration, PAHs, PCBs, Dredged sediments, Model comparison

## 1. Introduction

In harbours and natural or man-made waterways, dredging is required to maintain a sufficient depth for navigation and to prevent risks of flooding. Among the 65 million tons dredged per year in France, and according to French regulations (Decree of August, the 9<sup>th</sup>, 2006), 6 million tons are considered contaminated, as they exceed the S1 threshold (for fluvial sediment) and the N2 threshold (for marine sediment)(INERIS, 2009). In addition to the fact that they cannot be submerged, as they are considered waste, their contamination hampers their valorisation. The management of such dredged materials takes into account the technical feasibility, economics, applicable regulations and environmental acceptability of different options (re-use, disposal, processing) and receives considerable attention at an international level. Dredged materials are often disposed off on sites, acting as a source for hydrophobic organic contaminants (HOCs). However, in the sedimentary material, strong sorption to pyrogenic organic carbon, also known as black carbon (BC), tends to reduce the potential of the emission and the (bio)availability of HOCs (Cornelissen et al., 2005; Koelmans et al., 2006). Indeed, sorption to BC, such as diesel soot, coal soot, wood charcoal, or char-like carbonaceous particles, renders obsolete the traditional equilibrium partitioning theory (EPT) model assuming linear partitioning to amorphous organic matter (Bucheli and Gustafsson, 2000; Huang et al., 2003; Cornelissen et al., 2004; Cornelissen et al., 2005). Furthermore, a very high sorption capacity, similar or even higher than that of BC, has been previously reported for weathered mineral oil residues for polycyclic aromatic hydrocarbons (PAHs)(Jonker et al., 2003; Brändli et al., 2008) and polychlorinated biphenyls (PCBs) (Cornelissen et al., 2005; McNamara et al., 2005; Jonker and Barendregt, 2006). The sedimentary organic matter heterogeneity, especially the presence of BC and/or oil fractions, thus significantly affects HOC bioavailability and the risks to the environment (Huang et al., 2003; Cornelissen et al., 2005).

To assess HOC bioavailability, one approach consists of determining the freely dissolved pore water concentrations ( $C_{pw}$ ) (Reichenberg and Mayer, 2006; Cui et al., 2013). However, trace analysis of HOCs in porewater is a challenging task due to methodological difficulties, such as the separation of the porewater, the adsorption to the sampling equipment, the incomplete phase separation between particle-bound species (i.e., colloids and dissolved organic carbon) and concentrations lower than the detection limit (Hermans et al., 1992; Smedes, 1994; Hawthorne et al., 2009).

Thus, over the last decade, to overcome these analytical difficulties, methods based on passive sampling techniques have been developed to assess the freely dissolved concentrations of different HOCs in interstitial water (Stuer-Lauridsen, 2005; Allan et al., 2012; Cui et al., 2013). Passive samplers (mainly polymeric phases) are exposed to the sediment of interest, and the  $C_{pw}$  can then be determined, at equilibrium, from the amount of contaminant accumulated in the sampler. Several devices have been used to determine  $C_{pw}$  in sediment suspension: solid phase micro extraction (SPME) fibres coated with polydimethylsiloxane (PDMS) (Mayer et al., 2000; Heringa and Hermens, 2003; Cornelissen et al., 2008; Ghosh and Hawthorne, 2010), PDMS-coated vials (Reichenberg et al., 2008; Jahnke et al., 2012), polymer strips such as polyoxymethylene (POM) (Jonker and Koelmans, 2001; Cornelissen et al., 2008; Cornelissen et al., 2009), silicone rubber (Smedes et al., 2013) and low density polyethylene (LDPE) (Booij et al., 2003; Lohmann et al., 2005; Tomaszewsky and Luthy, 2008; Fernandez et al., 2009; Friedman et al., 2009; Allan et al., 2012). However, deducing the pore water concentration from passive sampling experiments requires checking various critical points for the validity of the experiment: mainly the attainment of equilibrium (contaminant desorption kinetics are not rate-limiting) and non-depletive conditions (the sorption capacity of the sampler is well below that of the sediment) (Huckins et al., 2006; Reichenberg and Mayer, 2006; Reichenberg et al., 2008). These validation requirements necessitate the selection of adequate sampler size, sediment volume and mixing mode.

The present study aims to determine the pore water concentration of PAHs (16) and PCBs (76) for four French and one Belgian highly contaminated dredged sediment by passive sampling experiments with LDPE strips exposed to saturated sediment under laboratory conditions. The experiments were designed to fulfil the validation requirements cited above. Performance reference compounds (PRC) spiked into the LDPE membranes prior to exposure were used to assess contaminant mass transfer and sediment depletion (Allan et al., 2012; Brand et al., 2012). After elimination of the data not satisfying the validation criteria, the sediment-pore water distribution coefficients ( $K_d$ ) were determined from the ratio of the experimental sediment concentrations ( $C_{sed}$ ) to the  $C_{pw}$ . The experimental  $K_d$  values were then compared with the theoretical  $K_d$  values obtained from various empirical and mechanistic distribution models used for risk assessments.

## 2. Materials and methods

**2.1. Reagents and glassware.** All solvents used for the extractions and analyses (n-hexane, acetone, cyclohexane and methanol) were of SupraSolv grade (Merck, Darmstadt, Germany). Individual analytical recovery standards, internal and PRC standards for the PAHs and PCBs, were obtained from Cluzeau Info Labo (Sainte Foy la Grande, France). The mixture standards (PAH Mix 16, PCB-mix1, PCB-mix 2 and PCB-Mix 3), provided by Dr. Ehrenstorfer Laboratories (Augsburg, Germany), were used for identification and quantification. Purities were > 99.5 % for PAHs and > 99.9 % for the deuterated PAHs. Analytical standards for PCBs were at a purity > 99.3 %. Glassware was solvent rinsed and heated overnight in a muffle furnace at 450 °C before use. MilliQ water (Option 15, Elga™) was used for the PRC spiking into LDPE membranes.

**2.2. Sediment sampling sites.** The five dredged sediment were collected from contaminated sites across France (Table 1) and were stored in 60 L barrels. Two of the five sediments were from marine harbours (Marseille and Dunkerque), two were from canals (Lens and Nimy Blaton) and one was from a highway sedimentation tank (Evry). The selected sediments were chosen to present contaminant concentrations higher than the S1 threshold (for fluvial sediment) and the N2 threshold (for marine sediment) according to French regulations on sediment dredging (Decree of August, the 9<sup>th</sup>, 2006) (Table S1). Approximately 1200 kg (wet weight) of sediment were collected per site. Sediment subsamples were sieved at 2 mm, homogenised and stored at room temperature in the dark before use.

**2.3. LDPE strip Preparation.** Lay-flat LDPE tubing was purchased from Brentwood Plastics Inc. (St. Louis, USA) and was reproducibly cut along the two side edges, resulting in 2.5 cm wide LDPE membranes (average membrane thickness of 80 µm). Five centimetre long strips were pre-extracted twice with cyclohexane for 24 h and then with methanol for 12 h. The spiking procedure consisted in exposing samplers to a 80:20 methanol/water bath fortified with a series of PRCs under agitation in the dark overnight (Booij et al., 2002). Anthracene-d<sub>10</sub>, fluoranthene-d<sub>10</sub>, chrysene-d<sub>12</sub>, benzo[a]pyrene-d<sub>12</sub>, dibenz [a,h]anthracene-d<sub>12</sub> and CB-10, CB-14, CB-29, CB-112, and CB-204, were selected for the PAH- and PCB-PRCs, respectively. These 10 PRCs

covered a log  $K_{ow}$  range from 4.53 (anthracene- $d_{10}$ ) to 7.3 (CB204). For each spiking batch, four strips were randomly sampled and extracted to determine the contamination level. The coefficient of variation (CV) ranged from 3 to 9 % within a batch, depending on the PRC considered. After spiking, the samplers were stored in clean jars at -20 °C until use.

**2.4. LDPE Exposure in Sediment Slurries.** Homogenised samples of saturated sediment were used for laboratory exposition. For each dredged location, seventeen glass jars were filled with 310 to 400 g of wet sediment (based on the density and water content) and one LDPE strip of 5 cm (0.09 g). The mass ratio between the membrane and the total organic carbon (TOC) were on average 0.0064, 0.0025, 0.0022, 0.0028 and 0.0076, for Marseille, Dunkerque, Lens, Nimy Blaton and Evry, respectively.  $C_{sed}$  and  $C_{pw}$  were both determined on the same samples. Exposure jars were closed with PTFE lined caps and placed on a rotating system (5 rpm) for a period of 46 days at 20 °C in the dark. LDPE strips were regularly sampled for kinetics studies after time periods of 1, 2, 4, 7, 10, 14, 18, 22, 25, 29, 32, 39 and 46 days. Analyses were performed in triplicate for the 14 and 46 day incubation times. For each sediment, unexposed LDPE strips were used as control samplers after 46 days. Control strips were treated according to the same analytical procedures as the exposed strips.

**2.5. Analysis of LDPE strips and Sediment characterisation.** After exposure, strips were washed with milli-Q water and extracted twice by soaking overnight in 100 mL cyclohexane. Recovery standards for the PAHs (acenaphthene- $d_{10}$ , pyrene- $d_{10}$ , perylene- $d_{12}$ ) and for the PCBs (CB-30, CB-145, CB-198) were added at the beginning of the first extraction step. Extracts were reduced to 500  $\mu$ L under a gentle stream of nitrogen. Cyclohexane extracts were then combined, and internal standards for PAHs (phenanthrene- $d_{10}$ , indeno[1,2,3-*c,d*]pyrene- $d_{12}$ ) and for PCBs (CB-78, Mirex) were added. Sediment characterisation consisted of the determination of the total concentration of PAHs and PCBs and of the oil, total organic and black carbon (BC) contents. For the determination of PAH, PCB and the oil content, approximately 3 g of dry weight homogenised sediment samples were extracted using an accelerated solvent extractor (ASE 350, Dionex). Further information about the analytical methods and quality control / quality assurance can be found in the supplementary material. An overview of the initial characterisation of the five

tested sediments is given in Table 1. Concentrations of the individual PAH and PCB congeners are given in Tables S2 and S3, respectively.

**2.6. Non-linear and linear Regression.** Non-linear and linear regressions were performed with Sigmaplot version 11 (Scientific computing, USA).

### 3. Results and discussion

**3.1. Contaminant Accumulation.** A measurable accumulation of PAHs and PCBs into the LDPE membranes was observed for all five sediments. The PAH and PCB concentrations from the control LDPE strips after 46 days of experiment were below detection limits. The accumulation process in the membrane obeys first order kinetics for all of the studied compounds as previously described by Huckins et al. (2006). The concentration in a membrane  $C_{LDPE}$  after a time (t) is expressed in equation 1:

$$C_{LDPE}(t) = C_{LDPE}^{eq} [1 - \exp(-k_e \cdot t)] \quad (1)$$

where  $C_{LDPE}^{eq}$  ( $\text{ng}\cdot\text{g}^{-1}$ ) is the concentration in the LDPE strip at equilibrium, and  $k_e$  ( $\text{d}^{-1}$ ) is the exchange rate constant. Data from recovery less than 85 % and greater than 115 % were ruled out. Approximately 7 % and 9 % of the data points had to be deleted for this reason for PAHs and PCBs, respectively.

The uptake curves fitted correctly with equation 1 with significant coefficients of determination for all contaminants (Fig. S1 for PAHs and Fig. S2 for PCBs). Triplicate analyses at day 14 and 46 showed good reproducibility with a relative standard deviation lower than 9 or 11 % for PAHs and PCBs, respectively. The exchange rates between the LDPE strips and water were calculated from equation 1 for each contaminant. Most of the contaminants (92 % and 96 % of PAHs and PCBs, respectively) had reached the equilibrium state after 46 days. Similar uptake curves have been previously reported by various authors (Booij et al., 2003; Allan et al., 2012; Smedes et al., 2013). After 46 days, the highest accumulated amounts of PAHs were found in LDPE membranes exposed to Lens sediment, whereas the lowest were for the Evry sediment. This result is correlated with the total sediment contamination level (Table 1).

As illustrated in Fig. 1 for the Lens sediment, the estimated exchange rate constant  $k_e$  is significantly correlated to the hydrophobicity of the compounds represented here by the logarithm of their octanol-water partition coefficient ( $\log K_{ow}$ ) for both native contaminants and PRCs. The highest rates of dissipation were observed for the most hydrophobic compounds (i.e., dibenz[*a,h*]anthracene for PAHs and CB-180 for PCBs). The exchange rate constants for the added PRCs and for the native contaminants are on the same order of magnitude. Similar results were obtained by Booij et al. (2003) and Allan et al. (2012) with LDPE strips exposed to harbour contaminated sediment. For an identical  $\log K_{ow}$ , higher exchange rate constant values were observed for PCBs, in comparison with PAHs, as illustrated by Fig. 1 for the Lens sediment and by Fig. S3 for the four other sediments. This difference could be explained by higher solubilities and differences in sorption mechanisms and interactions with the different sediment phases, as well as different diffusion coefficients in the LDPE membrane. Recently, Rusina et al. (2010) have shown strong relations between the logarithm of the diffusion coefficient ( $D$ ) and MW: for a given MW, higher diffusion coefficients were found for PCBs than for PAHs, confirming that the structure of the organic compounds affects the diffusion in the polymers.

**3.2. PRC exchange rate constants.** For each sediment, logarithms of the PRC dissipation rate  $\log k_e$  ( $d^{-1}$ ) values were plotted as a function of  $\log K_{ow}$  in Fig. 2 for PAHs and Fig. S4 for PCBs. The values obtained in this study were comparable to those reported for PRC by Booij et al. (2003) and Allan et al. (2012). Differences in the  $\log k_e$  values could be seen between the five sediments despite incubation under similar conditions. The highest  $\log k_e$  values were observed for Evry sediment for both PAHs and PCBs. The PRC exchange rate constants increased in the order of Nimy Blaton < Marseille < Lens < Dunkerque < Evry for both PAHs and PCBs. Recently, Smedes et al. (2013) have shown that the sediment content in suspension had a large influence on the uptake rate. According to those authors, the uptake rate increased with sediment content. In our study, the sediment concentrations were quite similar for all the five sediment and ranged from 0.40 (Lens) to 0.46 (Evry) g of sediment per g of suspension. The slight difference between sediment suspensions may explain the higher exchange rate constant observed for Evry. However, this parameter cannot explain the lower exchange rate constant observed for Nimy Blaton. Additionally, according to Booij et al. (2003), when resistance to the contaminant mass transfer into the membrane is much more related to the boundary layer process rather to the sampler itself, differences in the exchange rate constant could be the result of the sorption

properties of the sediment (particle size, porosity, TOC, BC, oil content). The highest log  $k_e$  values were indeed observed for the Evry sediment, which was characterised by a sandy texture with a low organic carbon content (Table 1). On the other hand, Nimy Blaton presented the lowest log  $k_e$  values, characterised by a clayed-silt texture with high organic carbon content.

**3.3. Depletion monitoring using Performance Reference Compounds.** According to Booij et al. (2003), to avoid contaminant depletion in sediment, two critical conditions regarding the experimental design should be met. The first one was that the buffering capacity of the sediment needs to be sufficient to ensure constant aqueous concentrations. In this respect, the contaminant amounts extracted from the sediment phase should be small compared with the initial amounts (< 1 %). The same authors proposed reducing the risk that the HOC desorption from the sediment suspension becomes rate-limiting by constraining the system to an LDPE/TOC mass ratio below 0.05 g.g<sup>-1</sup>. In other words, a ratio below 0.05 g.g<sup>-1</sup> would minimise contaminant depletion in the sediment as a result of absorption into the LDPE during sampler exposure. The present experiment was thus designed to fulfil both requirements, i.e., the absorbed amounts were lower than 1 % of the total quantity in the slurry for both PAHs and PCBs and the LDPE/TOC ratios were at least six times lower than 0.05 g.g<sup>-1</sup>.

Deducing the pore water concentration from this type of experiments requires checking whether a non-depletive situation was really obtained for the selected passive sampler. For that purpose, the sorption capacity of the sampler has to be negligible in comparison with that of the sediments. The depletion was monitored by the use of PRCs as proposed by Brand et al. (2012). If the sorption capacity of the sampler is negligible in comparison with that of the sediment, PRCs will release completely from the sampler. An incomplete release from samplers will indicate either that the equilibrium was not achieved or that the sediment phase was depleted. A distribution factor (DF) corresponding to the ratio of the amount of PRCs remaining in the membrane and the amount of PRCs in the sediment at equilibrium was calculated for all the PRCs in each exposure condition:

$$DF = C_{LDPE}^{PRC,eq} / C_{Sed}^{PRC,eq} \quad (2)$$



The DF values ranged from less than 0.02 for fluoranthene-D10 (Marseille sediment) to 1.68 for CB-204 (Evry sediment).

When the DF value is 0.1 or less, the sampler's sorption capacity is very small compared to that of the sediment. Consequently, the measured  $C_{pw}$  will not be significantly affected by the depletion of analytes in the sediment. In contrast, a higher DF value means that there is a small sorption capacity in the sediment and it is likely that the sampler has extracted a substantial fraction of the sediment's analytes and that the calculated  $C_{pw}$  value does not represent the "true" value (Brand et al., 2012). In such a case, the  $C_{pw}$  will be underestimated. For CB-204, we observed high distribution factors for NB and Evry, 0.99 and 1.68, respectively. In our experimental conditions, using LDPE strips, the exponential increase of DF with the  $\log K_{ow}$  could not be explained by a non-equilibrium state but rather by the result of both the sediment and membrane properties. High DF values mean that the sorption capacity in the sediment is lower than the one of the sampler and probably indicates that the membrane material has depleted the sediment (Brand et al. 2012). Additionally, very low diffusion coefficients in the LDPE membranes could also control the dissipation stage, especially for high molecular weight PRCs, and induce apparent equilibrium status (Rusina et al., 2007).

**3.4. Quality control of the data.** From the experimental PRC DF values and for each sediment, using  $DF=f(\log K_{ow})$  exponential regression models (Fig. S5), we calculated the DF values for all contaminants. We decided to keep data when the DF values were 0.1 or less for PAHs and 0.3 or less for PCBs. An underestimation of the pore water concentration by a maximum factor of 1.3 could be expected for PCBs. According to these requirements, data for PAHs with  $\log K_{ow} < 6.75$  were conserved for the five sediments. In the same way, PCBs with  $\log K_{ow} < 7.11$  were conserved for all sediments except for Evry, where the PCB data were considered for congeners with  $\log K_{ow} < 6.92$ . The difference observed for this latter sediment could be due both to the poor native concentration of PCBs and to its "sandy" structure associated with a low content of condensed organic carbon phase (Table 1). Consequently, in accordance with our "acceptance rule", approximately 20 % of the data points were not considered for the further work.

**3.5. Freely Dissolved Porewater Concentration.** Taking into account these validation requirements,  $C_{pw}$  values were then determined from the LDPE concentrations at equilibrium

according to equation 1. For the present work, the  $\log K_{LDPE-water}$  values for both PAHs and PCBs were calculated from MW according to Smedes et al. (2009), taking into account the chlorine position for PCBs.

The ranges of freely dissolved concentrations of PAHs and PCBs are presented in Table S4. For PAHs,  $C_{pw}$  ranged from 0.006 ng.L<sup>-1</sup> for dibenz [*a,h*]anthracene to 584.3 ng.L<sup>-1</sup> for naphthalene. For PCBs, the  $C_{pw}$  values were lower, ranging from 0.006 ng.L<sup>-1</sup> to 2.77 ng.L<sup>-1</sup>, respectively for CB-180 and CB-52. The concentrations of the present study were in the same range of magnitude of the values reported in the literature (Booij et al., 2003; Tomaszewsky and Luthy, 2008; Hawthorne et al., 2011; Allan et al., 2012). The sum of the freely dissolved PAH (14) concentrations increased in the following order: Evry < Dunkerque < Marseille < Nimy Blaton < Lens. Approximately 80 % of the total freely dissolved concentrations of PAHs were represented by the two and three aromatic ring congeners (Fig. S6). Among the various congeners, naphthalene accounted for more than 60 % of the dissolved PAHs, excepted for in the Lens sediment. The sum of the freely dissolved PCB (76) concentrations increased in the following order: Nimy Blaton < Lens < Dunkerque < Evry < Marseille. Although less abundant in the sediments, 3- and 4-Cl PCBs were responsible for more than 52 % of the total dissolved PCBs (Fig. S7).

**3.6. Distribution coefficients  $K_d$  and  $K_{TOC}$ .** From the validated pore water concentrations ( $C_{pw}^{Eq}$ ) and contaminant sediment concentrations ( $C_{sed}^{Eq}$ ) at equilibrium, we calculated the experimental  $K_d$  and  $K_{TOC}$  (total organic carbon-normalised distribution coefficients), according to equations 3 and 4.

$$K_{d,exp} (L_{pw}.kg^{-1}) = (C_{sed}^{Eq} / C_{pw}^{Eq}) \quad (3)$$

$$K_{TOC} (L_{pw}.kg_{TOC}^{-1}) = C_{sed}^{Eq} / (C_{pw}^{Eq} \cdot f_{TOC}) \quad (4)$$

We compared our experimental  $\log K_{TOC}$  values to the literature values from twelve references for PAHs and six references for PCBs. The  $K_{TOC}$  values obtained for the PAHs and PCBs by our method (LDPE) were consistent with the literature, with the  $\log K_{TOC}$ – $\log K_{ow}$  linear regressions

resulting in slopes close to 1 for both compound families (Fig. S8 for PAHs and Fig. S9 for PCBs).

Subsequently, we compared our observations of sediment-pore water partitioning to equilibrium expectations based on the sediment organic carbon content, assuming the well-documented relationship  $K_d = f_{\text{TOC}} \cdot K_{\text{TOC}}$ . The  $\log K_{\text{TOC}}$  of the PAHs and PCBs were calculated by the correlation with the  $\log K_{\text{ow}}$  established by Schwarzenbach et al. (2003). The  $\log K_{d,\text{exp}}$  values observed were systematically higher than the calculated values from  $\log K_{\text{ow}}$ . The divergence of the  $\log K_{d,\text{exp}}$  values were highest for PAHs (1.5 – 1.9 log unit). The  $K_{d,\text{exp}}$  values for the PCBs were higher than the calculated values by approximately 1 log unit. As previously reported (Cornelissen et al., 2005; Allan et al., 2012), adsorption by total organic carbon ( $f_{\text{TOC}}K_{\text{TOC}}$ ) is not sufficient to explain the sorption of native organic contaminants in these five sediments. These findings highlight the need to consider the nature of the sedimentary organic matter and, in particular, to distinguish the different phases presenting different sorption capacities.

**3.7. Partitioning model and experimental  $K_d$  values.** Currently, two types of partitioning models are used in the literature to describe the sorption capacity of the sediment: (i) mechanistic approaches mainly by accounting for the contribution of all sorbents, and (ii) empirical approaches mainly by accounting for physicochemical properties of the contaminant and sorption properties of one specific BC selected phase (coal tar, activated carbon) (Arp et al., 2009).

For mechanistic approaches, the distributions of HOCs were evaluated using the double and triple domain sorption model (Eq. 5 and 6).

$$K_d = f_{\text{AOC}} \cdot K_{\text{AOC}} + f_{\text{BC}} \cdot K_{\text{BC}} \cdot C_{\text{pw}}^{n-1} \quad (5)$$

$$K_d = f_{\text{AOC}} \cdot K_{\text{AOC}} + f_{\text{Oil}} \cdot K_{\text{Oil}} + f_{\text{BC}} \cdot K_{\text{BC}} \cdot C_{\text{pw}}^{n-1} \quad (6)$$

in which  $f_{\text{AOC}}$  ( $f_{\text{AOC}} = f_{\text{TOC}} - f_{\text{BC}}$ ),  $f_{\text{Oil}}$ , and  $f_{\text{BC}}$  are the amorphous organic carbon, oil, and black carbon weight fractions ( $\text{kg} \cdot \text{kg}^{-1}$ ), respectively (Table 1).

$K_{\text{AOC}}$  ( $\text{L} \cdot \text{kg}^{-1}$ ),  $K_{\text{Oil}}$  ( $\text{L} \cdot \text{kg}^{-1}$ ), and  $K_{\text{BC}}$  ( $\text{L} \cdot \text{kg}^{-1}$ ) are the sorption constants for these respective phases. The model described in Eq.6, recently proposed by Koelmans et al. (2009), takes into account the high sorption capacity of weathered oil. According to Jonker et al. (2003), oil can behave as an additional sorbent when the oil content approximates 10 to 30 % of the total organic carbon weight basis (corresponding to the Critical Separate Phase Concentration - CSPC). For the

studied sediment, the mass ratio between the oil and TOC content ranged from 6 % to 14 % for NB and Evry (Table 1). The triple domain sorption model was thus applied for the sediment from Marseille, Dunkerque and Evry with respective oil/TOC ratios of 11 %, 11 % and 14 %.

The sorption distribution coefficients considered for each model were calculated from compound-class specific regressions with  $\log K_{ow}$ .  $\log K_{AOC}$  values were calculated according to Schwarzenbach et al. (2003), and  $\log K_{BC}$  or  $\log K_{oil}$  were calculated from the  $\log K_{ow}$  (Eq. 7 to 14), as presented in Table 2. The chromatographic analysis of the aliphatic hydrocarbons in all sediment revealed an advanced state of oil degradation with the presence of large unresolved complex mixtures (UCMs) (Wang et al., 2011). Therefore, we considered  $K_{oil}$  values for weathered oil (Eq. 9, 10 and 14). The Freundlich exponent ( $n$ ) for nonlinear sorption to BC was set to 0.7 for PAHs (Eq. 7 and Eq. 8) as proposed by Hawthorne et al. (2007) and Koelmans et al. (2009). For PCBs,  $n$  was also set to 0.7 (Eq. 12 and Eq. 13), as previously reported by several authors (Accardi-Dey and Gschwend, 2002; Moermond et al., 2005; Pikaar et al., 2006; Koelmans et al., 2009) and to 1 (linear sorption isotherm), as proposed by Werner et al. (2010), for equation 11.

For the empirical approach, we tested the “coal tar model”, considered as the most appropriate polyparameter linear free-energy relationship (PP-LFER) based on the Abraham’s solvation parameters (Arp et al., 2009; van Noort et al., 2010). Additionally, we also compared our set of data to the Raoult’s Law model, using coal tar as the sorbent phase. For PCBs, and for both models, we added a specific term based on the abundance ratio of the PCB congeners (WF), as a proxy for weathering, aiming for a better correlation (Hawthorne et al., 2011). WF ranged from 0 to near 1, respectively, for fresh to weathered contamination. From experimental concentrations of CB 28, 52 and 153, we obtained WF of 0.60, 0.75, 0.83, 0.86 and 0.96, for Evry, NB, Lens, Dunkerque and Marseille sediment, respectively.

Experimental data from Marseille, Dunkerque and Evry sediment were tested with the double and triple domain sorption model, whereas Lens and NB were tested with the double domain sorption model for the validation of the best combination among equations 7 to 14 in Table 2. All experimental data were tested with both empirical models. Models were considered successful for the prediction of average  $\log K_d$  or  $\log K_{TOC}$  when 90 % and 99 % of the computed values were

contained in the respective ranges of  $\pm 1$  log (factor  $\pm 10$ ) and of  $\pm 1.5$  log (factor of  $\pm 30$ ) (Arp et al., 2009; Hawthorne et al., 2011).

For PAHs, among the tested models, the best results were obtained for empirical models and particularly for Raoult's Law model (Fig. 3). This model predicted  $\log K_{\text{TOC}}$  values in the ranges of  $\log \pm 1$  and  $\pm 1.5$  with frequencies of 91 % and 100 %, respectively. The mean deviation was  $-0.39 (\pm 0.52)$ , showing on average a slight underestimation of  $\log K_{\text{TOC}}$ . The  $K_{\text{Oil}}$  values for the PAHs were estimated using a  $\log K_{\text{Oil}}\text{-Log } K_{\text{ow}}$  regression (Eq. 9) for compounds presenting  $\log K_{\text{ow}}$  ranging from 4.6 to 6.9, as previously described by Koelmans et al. (2009). Considering this  $\log K_{\text{ow}}$  range, the  $K_{\text{d}}$  experimental values were properly predicted by the triple domain sorption model (Eq. 6) using Eq. 7 and Eq. 9 (Table 2). The slope of the linear regression  $\log K_{\text{d,pred}}\text{-log } K_{\text{d,exp}}$  was close to 1, and all the computed values were contained in a range of  $\pm 1$  log (factor of 10) (Fig.S10). From this mechanistic approach, it was possible to evaluate the PAH sorption to different organic phases of the sediment. As illustrated for the Lens sediment in Fig. S11, the less hydrophobic PAHs were preferentially sorbed to the oil fraction, whereas the most hydrophobic PAHs were mainly sorbed to BC.

On the other hand, the mechanistic model exhibited better results for PCBs (Eq. 6) with estimation of  $K_{\text{BC}}$  from Eq. 12 and  $K_{\text{Oil}}$  from Eq. 14 for the Marseille, Dunkerque and Evry sediments. As illustrated for the Lens sediment in Fig. S11, PCB congeners were mainly sorbed to BC (up to 50 %), and the oil fraction accounted for 10 to 30 % of sorption, depending on the congeners.

Although the ratio for the NB and Lens sediments were lower than the supposed CSPC values discussed above, the triple domain sorption model was successfully applied to the Lens and Nimy Blaton sediment, which also presented important oil contents (6310 and 9580  $\text{mg.kg}^{-1}$ , respectively). The observed values were all included in the factors of 10 (Fig. 3). This approach presented a significant correlation with the experimental values ( $R^2 = 0.69$ ) with a deviation on average of  $0.12 \pm 0.33$ . Experimental distribution coefficients for the PCB values for the NB and Lens sediments were well-described by the triple domain sorption, despite an oil/TOC mass ratio lower than the CSPC values. These findings could be explained by the fact that the CSPC value was determined by Jonker et al. (2003) for a unique oil-spiked and weathered sediment with a

low organic content (<1 %). The behaviour of real decades-weathered sediment could be notably different in terms of native contaminant desorption (Chai et al., 2006). In fact, the presence of separate phases would be a function of the oil content but also of the type and the amount of organic carbon (Jonker and Barendregt, 2006) and the presence of clay-humic complexes (Lu et al., 2006). This reveals the need for a better assessment of the CSPC value used to define the applicability limits of the model. The different types of organic carbon must be taken into account. To this end, the molecular weight could give some valuable information. Thus, a better estimation of the CSPC could be achieved by using molar-based in place of mass-based values. This calls for further work in this domain.

#### **4. Conclusion**

Passive sampling with LDPE strips is suitable for measuring the pore water concentrations and assessing the sorption capacity (sediment/pore water distribution coefficient) of various contaminated sediments. For the studied compounds, in view of an operational approach (risk assessment/remediation), it was difficult to use a predictive model to determine  $C_{pw}$  because of the large number of literature models (both empirical and mechanistic) and regressions (choice of the partitioning coefficient for a specific sorbent phase). Nevertheless, acceptable correlations between model predictions and experimental data were obtained for five different and distinct sediments. Reliable predictive relationships for PAH partitioning were obtained by Raoult's Law model using the physicochemical properties of each contaminant (water solubility) and coal tar sorbent phase concentration. For PCBs, triple domain sorption (amorphous organic carbon, black carbon and oil phases) could model the data successfully. The differences observed for the PCB phase distribution in the five sediments could be explained by the type and source of the organic matter. Nevertheless, particularly under a regulatory framework, it is important to obtain a more reliable estimation of CSPC to better assess the applicability limits of the triple domain sorption model. To this end, and to improve the robustness of both models, substantial additional work is required. Moreover, in most cases, the use of such models implies a thorough knowledge of the sediment composition. Although, to date, no analytical consensus was found for the choice of a

specific method for the determination of the porewater concentration, the direct measurement seems to be more accurate and thus, preferable.

## **5. Acknowledgements**

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## **Appendix A. Supplementary information**

Quality threshold values for dredging according to the French regulation for PAH and PCB, PCB and PAH sediment concentrations for all sediments; accumulation of five PAHs and PCBs in LDPE membrane exposed to Lens sediment; correlation between the exchange rate constant ( $\log k_e$ ) with the molecular weight for the five contaminated sediments for PAHs; the first-order dissipation rate constant ( $\log k_e$ ) of PCB PRCs into LDPE membrane samplers for the five sediments; the distribution factor for PAH PRCs and PCB PRCs as a function of  $\log K_{ow}$  for Lens sediment; the ranges of pore water concentrations for the studied PAHs and the seven indicator PCBs; the fingerprint of the PAHs and PCBs concentrations in pore water and in sediment; positioning  $\log K_{TOC}$  values for PAHs and PCBs for the five sediments among the  $\log K_{TOC}$  values from literature; the triple sorption model correlation for PAHs and the PAHs and PCBs distribution among AOM, BC and Oil sorbent phases are available in the supporting information.

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# **Polyethylene passive samplers to determine sediment-porewater distribution coefficients of persistent organic pollutants in five heavily contaminated dredged sediment**

Benoit Charrasse, Céline Tixier, Pierre Hennebert and Pierre Doumenq

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**Table 2.** Relationships between  $K_{BC}$ ,  $K_{oil}$  and  $K_{ow}$  for PAHs and PCBs.

**Table 1.** Initial characterization of the five tested sediments including: black carbon (BC) and total organic carbon (TOC) content; contaminant concentration; total hydrocarbons content (Oil) and texture.

	Unit	Evry	Dunkerque	Lens	Marseille	Nimy Blaton
Origin		HST <sup>1</sup>	Marine harbor	Canal	Marine harbor	Canal
Localization		48°36'34.99''N 2°25'56.15''E	51°2'33.01''N 2°21'34.36''E	50°26'13.77''N 2°53'0.24''E	43°19'21.50''N 5°21'37.05''E	50°30'9.26''N 3°41'56.53''E
Sample depth	m	2	8	7	10	6
BC - black carbon	%	0.00	0.06	0.66	0.22	0.35
TOC	%	3.20	2.85	13.9	4.93	10.6
∑ 14 PAH <sup>2</sup>	µg kg <sup>-1</sup>	2550	7710	45700	37100	3360
∑ 7 PCB <sup>3</sup>	µg kg <sup>-1</sup>	75	541	539	3530	318
Oil (C <sub>10</sub> -C <sub>40</sub> )	mg kg <sup>-1</sup>	4590	3170	9580	5340	6310
Oil /TOC	%	14.3	11.1	6.9	10.8	6.0
Texture		Sandy-silty	Silty-sandy	Clayey silt	Silty-sandy	Clayey silt

<sup>1</sup>highway sedimentation tank

<sup>2</sup>naphthalene, acenaphthene, acenaphthylene, fluorene, phenanthrene, anthracene, fluoranthene, pyrene, chrysene, benz[*a*]anthracene, benzo[*a*]pyrene, indeno[1,2,3-*c,d*]pyrene, dibenz[*a,h*]anthracene, benzo[*g,h,i*]perylene

<sup>3</sup> CB28, CB52, CB101, CB118, CB138, CB153, CB180

**Table 2.** Relationships between  $K_{BC}$ ,  $K_{oil}$  and  $K_{ow}$  for PAHs and PCBs.

Studied contaminant	Equation	Relationships f(log $K_{ow}$ )	References
PAHs	7	$\text{Log}K_{BC} = 1,6 \text{ log}K_{ow} - 1,4$	(Schwarzenbach et al., 2003)
PAHs	8	$\text{Log}K_{BC} = 0,6997 * \text{log}K_{ow} * + 2,8219$	(Koelmans et al., 2006)
PAHs	9	$\text{Log}K_{oil} = 0,1287 * \text{log}K_{ow} * + 6.2943$	(Koelmans et al., 2009)
PAHs	10	$\text{Log}K_{oil} = 0,9052 * \text{log}K_{ow} * + 0.9079$	(Jonker et al., 2003)
PCBs	11	$\text{Log}K_{BC} = 0,912 * \text{log}K_{ow}^{**} + 1,370$	(Werner et al., 2010)
PCBs	12	$\text{Log}K_{BC} = 1,016 * \text{log}K_{ow}^{**} + 0,2469$	(Koelmans et al., 2006)
PCBs	13	$\text{Log}K_{BC} = 0,980 * \text{log}K_{ow}^{**} + 0,491$	(Moermond et al., 2005)
PCBs	14	$\text{Log}K_{oil} = 0,9948 * \text{log}K_{ow}^{**} + 0,9787$	(Jonker and Barendregt, 2006)

\*PAH  $\text{log}K_{ow}$  from Mackay et al. (1992); \*\*PCB  $\text{log}K_{ow}$  from Hawker and Connell. (1988)

# Polyethylene passive samplers to determine sediment-porewater distribution coefficients of persistent organic pollutants in five heavily contaminated dredged sediment

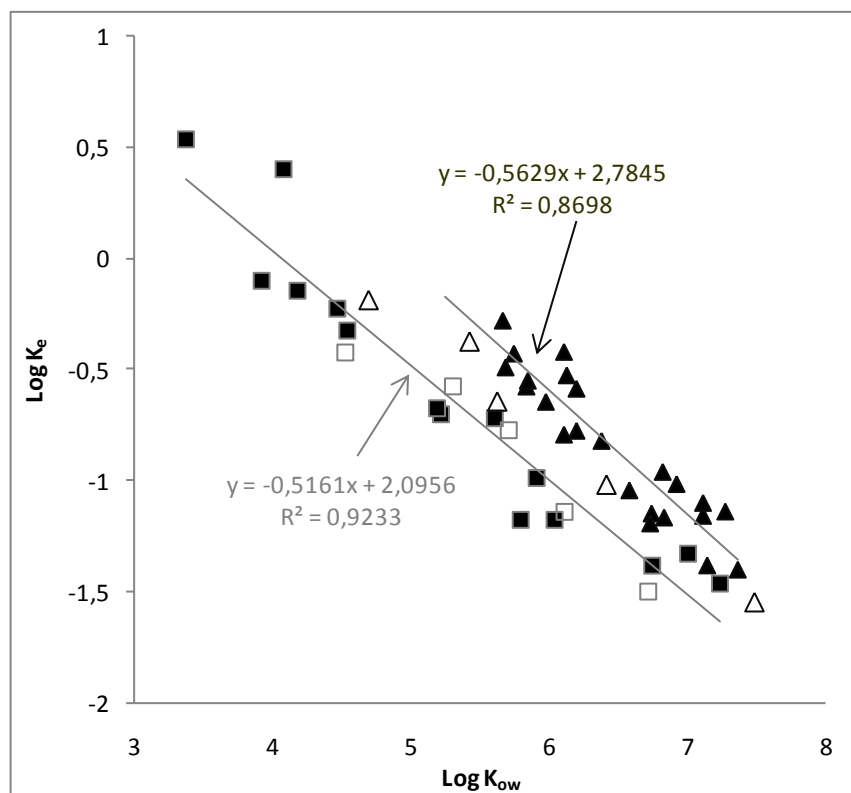
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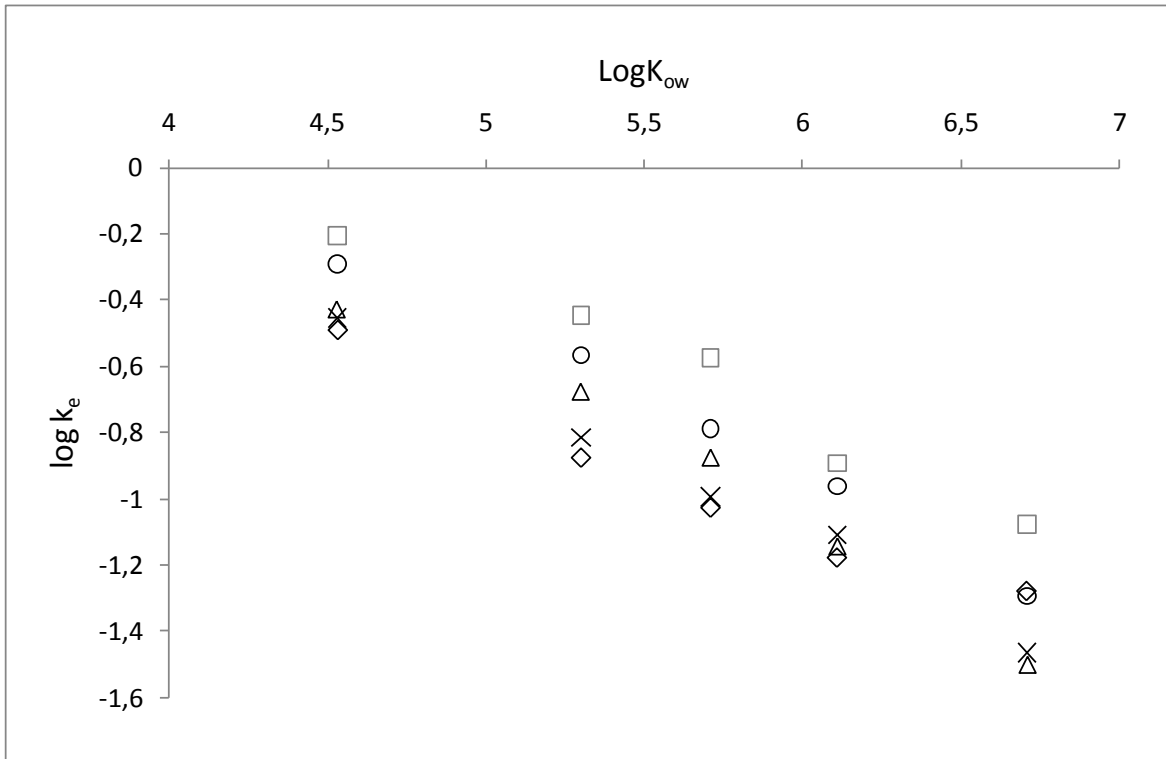
**Fig.2.** First-order dissipation rate constant ( $\log k_e$ ) of PAH PRCs into LDPE membrane samplers for □ Evry, ○ Dunkerque, △ Lens, × Marseille and ◇ NB sediments

**Fig.3.** The solid line is 1:1 Modeled  $\log K_d / \log K_{TOC}$  against experimental  $\log K_d / \log K_{TOC}$  for the five studied sediments for PAHs (on the left, considering with Raoult's Law model) and for PCBs (on the right, considering triple sorption model). The solid line is 1:1. The internal dashed lines represent the domain suitable for a factor of 10 (1 log difference). The external dashed lines correspond to the domain suitable for a factor of 30 ( $\approx 1.5$  log difference)

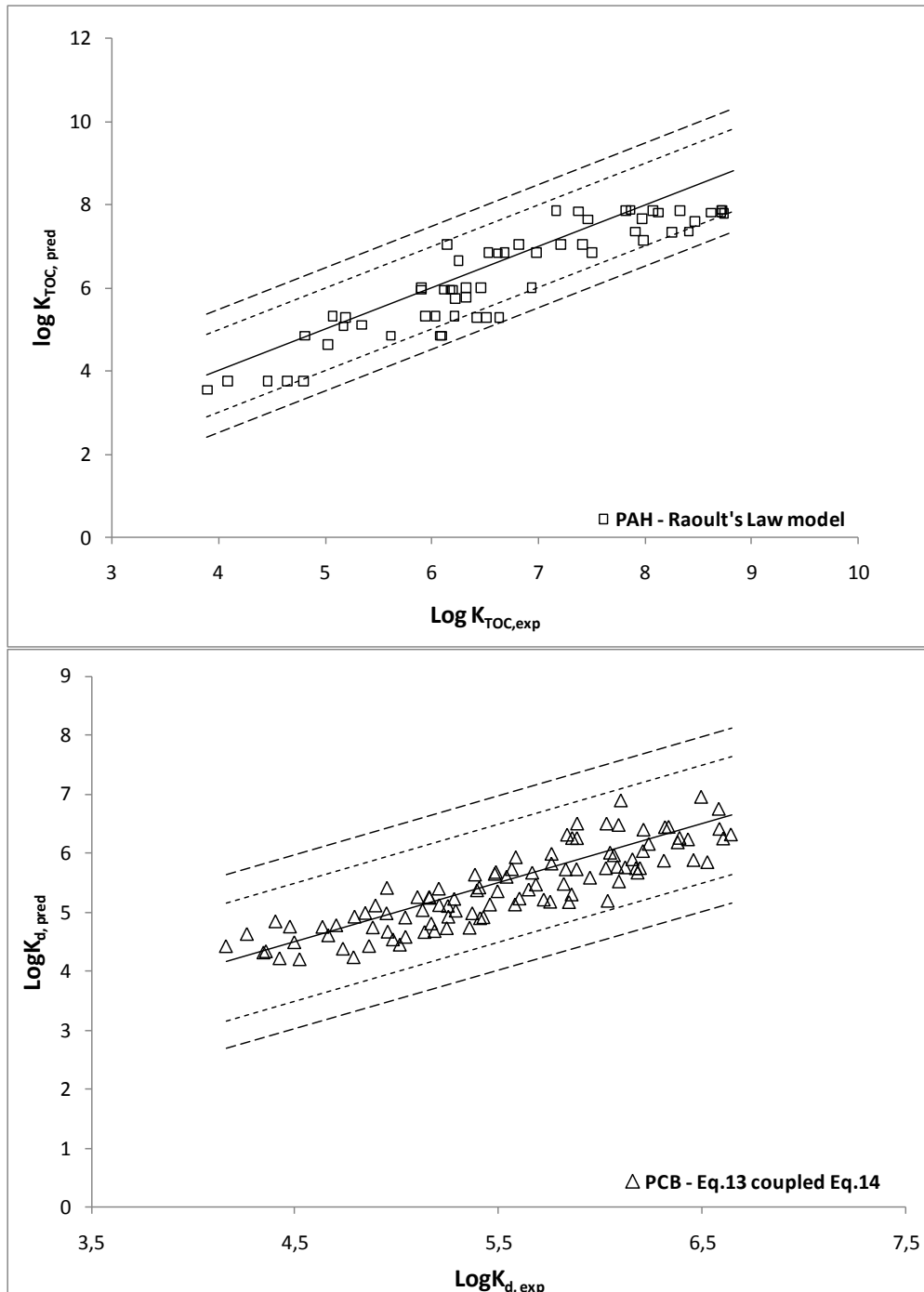


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**Fig.2.** First-order dissipation rate constant ( $\log k_e$ ) of PAH PRCs into LDPE membrane samplers for  $\square$  Evry,  $\circ$  Dunkerque,  $\triangle$  Lens,  $\times$  Marseille and  $\diamond$  NB sediments



**Fig.3.** The solid line is 1:1 Modeled  $\text{Log } K_d / \text{Log } K_{TOC}$  against experimental  $\text{Log } K_d / \text{Log } K_{TOC}$  for the five studied sediments for PAHs (on the left, considering with Raoult's Law model) and for PCBs (on the right, considering triple sorption model). The solid line is 1:1. The internal dashed lines represent the domain suitable for a factor of 10 (1 log difference). The external dashed lines correspond to the domain suitable for a factor of 30 ( $\approx 1.5$  log difference).