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Geochemistry, Geophysics, Geosystems

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Supporting Information for

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Correction of interstitial water changes in calibration methods applied to XRF core-scanning major elements in long sediment cores: case study from the South China Sea

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22 **Introduction**

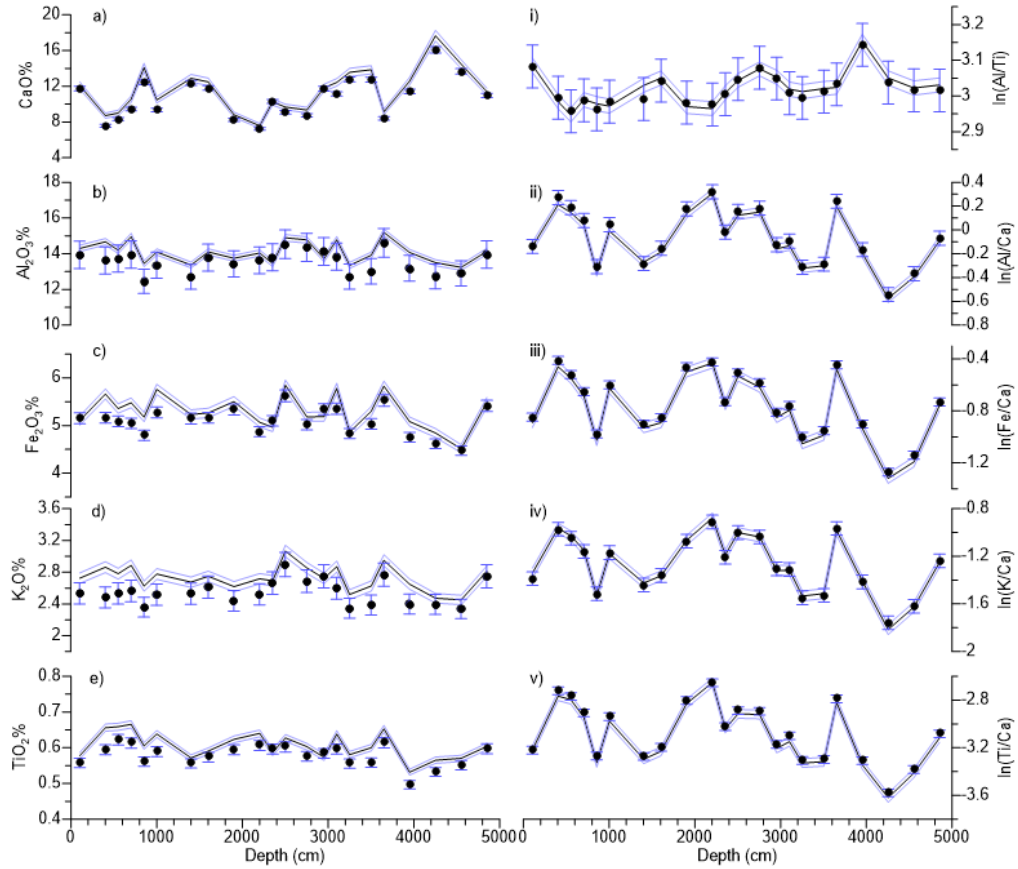
23 The reliability of WD-XRF concentrations used as reference datasets for XRF scanning
24 calibration is evaluated in text S1. The detailed descriptions of existing and improved
25 calibrations are introduced in text S2 and S3, respectively. The data used in the XRF
26 scanning calibrations and in the evaluation of calibration methods are included in the
27 supplemental data set S1 and S2. Data set S3 presents the ICP-AES analyses that are
28 used to verify the accuracy of WD-XRF measurements.
29

30 Text S1. Accuracy evaluation of WD-XRF element concentrations

31 The WD-XRF analysis of major elements has been reported to be of high accuracy by various
32 studies [e.g. Tsuchiya et al., 1989; Rousseau et al., 1996; Rahmani et al., 2004; Gazulla et al., 2013;
33 Hunt et al., 2014]. Therefore, quantitative element concentrations obtained by energy-dispersive
34 or wavelength-dispersive XRF have been used as reference datasets for correcting or calibrating
35 XRF-scan intensities in several previous studies [e.g. Tjallingii et al., 2007; Weltje and Tjallingii,
36 2008; Hennekam and De Lange, 2012]. To further confirm the reliability of WD-XRF
37 concentrations used as reference datasets in this study, inductive coupled plasma atomic
38 emission spectrometer (ICP-AES) analyses were performed on 22 discrete samples. Dried and
39 ground bulk sediments were heated at 600°C for 4 hours to remove organic matter. Their weights
40 were measured before and after heating to calculate the loss on ignition (LOI). The sediments,
41 together with a series of Chinese rock and sediment standards (*i.e.* GSR5, GSR6 and GSD9), were
42 digested in HF+HNO₃ mixed acid. Major elements were then measured on an IRIS Advantage
43 ICP-AES. The mean relative accuracy estimated from the Chinese rock and sediment standard
44 samples is better than 4%.

45 WD-XRF concentrations of six major-element oxides are plotted together with ICP-AES data
46 in Fig S1. The associated uncertainties account for the instrument analysis. Because
47 concentrations in bulk sediments are considered, the 1% analytical uncertainty of LOI [Heiri et al.
48 2001] is also taken into account in ICP-AES uncertainties.

49 WD-XRF and ICP-AES concentrations are very consistent within the analytical uncertainties
50 and they follow the same variation patterns [Fig. S1a-S1e]. We observe that the ICP-AES
51 concentrations are slightly shifted with respect to the WD-XRF concentrations for all five
52 elements. This may be due to the fact that Si is not measured by the ICP method but deduced
53 from the measurement of all other elements and LOI. The observed shifts may therefore result
54 from erroneous Si evaluation. In addition, the log-ratio values and variations are identical in the
55 two datasets [Fig. S1i-S1v], indicating that the relative proportions of elements are exactly the
56 same, no matter the method (ICP-AES or WD-XRF) used to measure the element concentrations.
57 Because the WD-XRF analytical method allows direct measurements of Si concentrations (which
58 account for about 50% of the geochemical composition of bulk sediments in this study), we
59 prefer to use here WD-XRF measurements as reference datasets for the calibration of
60 geochemical concentrations in core MD12-3432.



61
 62 **Figure S1.** Comparison of ICP-AES and WD-XRF results in terms of oxide concentrations of a)
 63 CaO, b) Al₂O₃, c) Fe₂O₃, d) K₂O, and e) TiO₂, and of log-ratios i) ln(Al/Ti), ii) ln(Al/Ca), iii) ln(Fe/Ti),
 64 iv) ln(K/Ca), and v) ln(Ti/Ca). ICP-AES results (black lines) are plotted with their analytical
 65 uncertainties (blue lines), and WD-XRF results (black dots) are plotted with analytical
 66 uncertainties (blue error bar).

67 Text S2. Description of existing XRF calibration methods

68 S2.1 Correction for water absorption effect

69 Based on high-resolution analysis of three short sediment sequences, [Hennekam and De](#)
70 [Lange \[2012\]](#) proposed a routine approach to correct the influence of water absorption on log-
71 ratios of XRF-scan intensities due to variations in water film thickness. According to the Lambert-
72 Beer law [[Hubbell, 1982](#)] that describes the relationship between original intensity and residual
73 intensity of a specific X-ray before and after passing through a homogeneous medium, the
74 original intensity $I_{e,d}'$ of element e at depth d can be obtained following equation S1 by assuming
75 that CI intensity changes only represent variations in water film thickness:

$$76 \quad I_{e,d}' = I_{e,d} \exp(\mu_{e,CI} I_{CI,d}) \quad (\text{eq S1})$$

77 where $I_{e,d}$ is the intensity obtained for element e at depth d by XRF scanning, $\mu_{e,CI}$ is the specific
78 attenuation coefficient for element e , and $I_{CI,d}$ is the XRF scanning CI intensity at depth d . $\mu_{e,CI}$
79 is empirically obtained by changing its value to reach an optimal linear correlation between
80 corrected XRF-scan intensities and WD-XRF concentrations of the target element.

81 In the case of core MD12-3432, the entire WD-XRF dataset (102 samples) was used to
82 determine the $\mu_{e,CI}$ value for each element. The NMS and MLC methods (named as W_NMS and
83 W_MLC) were then performed on the water-corrected intensities.

84

85 S2.2 Normalized median-scaled calibration (NMS)

86 In the NMS method [[Lyle et al., 2012](#); [Lyle and Backman 2013](#)], XRF-scan intensities are first
87 scaled to the range of sedimentary component concentration values, independently for each
88 element. Indeed, various elements do not have the same efficiency of producing characteristic
89 X-ray, and normalizing on XRF-scan intensities would, therefore, produce awry relative
90 proportions with respect to the element compositions. The median-scaled value of an element
91 component e at depth d ($S_{e,d}$) is:

$$92 \quad S_{e,d} = W_{e,M} \times I_{e,d} / I_{e,M} \quad (\text{eq S2})$$

93 where $W_{e,M}$ is the median concentration of the corresponding sedimentary component e from
94 the WD-XRF calibration dataset, $I_{e,d}$ is the XRF-scan intensity of element component e at depth
95 d , and $I_{e,M}$ is the median intensity value of element component e over the entire XRF-scan dataset.

96 In a second step, the median-scaled values are summed and normalized to 100% to
97 eliminate the variability caused by differences in density and cracks. The normalized median-
98 scaled value of element component e at depth d ($NMS_{e,d}$) is calculated as:

$$99 \quad NMS_{e,d} = S_{e,d} \times 100\% / \sum S_d \quad (\text{eq S3})$$

100 where $S_{e,d}$ represents the median-scaled value of element component e at depth d , and $\sum S_d$ is
101 the sum of median-scaled values of the six sedimentary components at depth d .

102 Finally, normalized median-scaled values are calibrated against WD-XRF concentrations of
103 sedimentary components through linear regression equations, providing high-resolution
104 calibrated concentrations of each sedimentary component in bulk sediments.

105

106 S2.3 Multivariate log-ratio calibration (MLC)

107 MLC [[Weltje et al., 2015](#)] is developed from the previously proposed log-ratio calibration
108 equation (LRCE) approach [[Weltje and Tjallingii, 2008](#)]. The use of centered log-ratios (clr) and
109 partial least squares regression allows the MLC method to take account of multiple covariances
110 at the same time [[Weltje et al., 2015](#)]. Therefore the MLC method can directly fit the absorption
111 and enhancement of intensities caused by the presence of unmeasured elements. Benefiting
112 from the multivariate calibration, MLC can also predict bulk element concentrations by including
113 the union of unmeasured elements as one "element" [[Weltje et al., 2015](#)]. Moreover, the

114 improved workflow, which includes uncertainty estimation and automatic selection of
115 calibration samples, enhances the predictive power of the MLC method [Weltje et al., 2015].

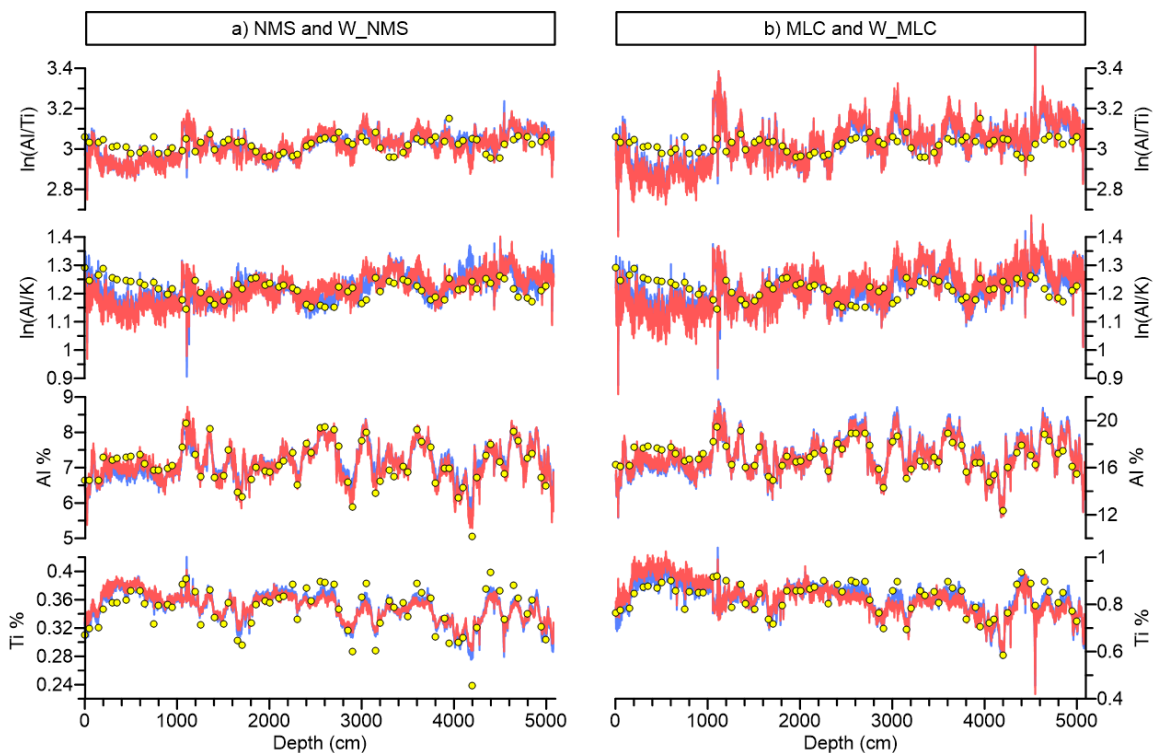
116 To perform the MLC, XRF-scan element intensities and WD-XRF element concentrations are
117 first transformed to centered log-ratios, and then scaled with the inverse of their uncertainties
118 determined from replicate measurements. The calibration dataset can be automatically
119 determined using a hierarchical cluster analysis of the scaled clr-transformed intensities. A
120 reasonable model of calibration is then carried out using the calibration dataset by means of
121 partial least squares regression, and is applied to the entire XRF-scan dataset for calibration. The
122 calibration approach has been implemented in the XELERATE software available on line
123 [www.ascar.nl].

124 S2.4 Comparison between NMS and W-NMS results and between MLC and W-MLC results

125 The water absorption correction (described in text S2.1) improves the accuracy of NMS- and
126 MLC-calibrated results by reducing their MSRE [Table S1]. Moreover, as indicated by the
127 increased average R^2 [Table S1], applying the water absorption correction improves their
128 correlation to WD-XRF concentrations. Therefore, W_NMS and W_MLC are discussed in the
129 main text (section 5).

130 However, calibrated W_NMS and W_MLC results remain quite similar to the original NMS
131 and MLC calibrated results, respectively, and deviations from WD-XRF concentrations data
132 are still observed for all methods in the top sections of core MD12-3234 [Fig. S2]. This comparison
133 confirms our conclusions (section 5.3 of the main text) that the water absorption correction is
134 insufficient to correct downcore water changes in our case study.
135

136



137

138 **Figure S2.** Calibration results. NMS (red lines) and W_NMS (blue lines) results are shown in the
139 left panel (a), MLC (red lines) and W_MLC (blue lines) results are presented in the right panel (b).
140 WD-XRF evaluation data are shown as yellow dots. Note that Al% and Ti% calibrated by MLC and
141 W_MLC refer to relative proportions of Al and Ti.

142

143 **Text S3. Description of proposed improved calibration methods**

144 S3.1 Normalized polynomial-scaled calibration (NPS)

145 In the NPS approach, the polynomial-scaled value of element component e at depth d is first
146 calculated by the equation S4:

$$147 \quad PS_{e,d} = (a' \times d^2 + b' \times d + c') \times I_{e,d} / (a \times d^2 + b \times d + c) \quad (\text{eq S4})$$

148 where $I_{e,d}$ is the XRF-scan intensity of element component e at depth d ; a , b , c and a' , b' , c' are the
149 coefficients of quadratic polynomials fitted through the XRF-scan intensities and WD-XRF
150 concentrations of element component e , respectively [Table S2].

151 In the second step, this polynomial-scaled value is normalized to the sum of WD-XRF
152 concentrations for all element components, instead of to unity as in the NMS, because the sum
153 of all component concentrations is diluted by components that are not included in the calibration
154 (e.g. organic matter, Na and Mg) and varies below 90% along the core. As the calibration dataset
155 is smaller than polynomial-scaled dataset, WD-XRF concentration sums are interpolated to fit
156 the polynomial-scaled dataset. The normalized polynomial-scaled value of element component
157 e at depth d is then determined using the following equation:

$$158 \quad NPS_{e,d} = \sum W_d \times PS_{e,d} / \sum S_d \quad (\text{eq S5})$$

159 where $\sum W_d$ is the interpolated sum of WD-XRF concentrations for all element components at
160 depth d , $PS_{e,d}$ is obtained by equation S4, and $\sum S_d$ is the sum of polynomial-scaled values of all
161 element components at depth d .

162 Finally, normalized polynomial-scaled data are calibrated against WD-XRF concentrations
163 for the six chosen major element components using linear regression equations.

164

165 S3.2 Polynomial corrected multivariate log-ratio calibration (P_MLC)

166 In the polynomial-corrected MLC (P_MLC) approach, XRF-scan element intensities are first
167 summed to unity. A polynomial correction is then performed in log-ratio space on all possible
168 ratio combinations. The polynomial-corrected log-ratio of element e and D at depth d ($P_{eD,d}$) is
169 calculated using equation S6:

$$170 \quad P_{eD,d} = (a' \times d^2 + b' \times d + c') + \ln(I_{e,d} / I_{D,d}) - (a \times d^2 + b \times d + c) \quad (\text{eq S6})$$

171 where $I_{e,d}$ and $I_{D,d}$ are normalized XRF-scan intensities of element e and D at depth d ; a , b , c and
172 a' , b' , c' are the coefficients of quadratic polynomial fitted through the XRF-scan intensities and
173 WD-XRF element concentrations, respectively [Table S2].

174 All polynomial-corrected log-ratios are then tested to select the element used as common
175 denominator in log-ratios in order to obtain the most robust correction. In this case of core MD12-
176 3432, Ca is chosen as the common denominator. An inverse additive log-ratio transformation is
177 then performed on the polynomial-corrected log-ratios with Ca as common denominator,
178 transforming them to relative proportions of intensities. The transformed dataset is further
179 calibrated using the MLC approach.

180

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233

| | MSRE | R ² | | | | | | |
|-------|---------|----------------|------|------|------|------|------|---------|
| | | Al | Si | K | Ca | Ti | Fe | Average |
| NMS | 0.00250 | 0.92 | 0.96 | 0.78 | 0.98 | 0.68 | 0.45 | 0.80 |
| MLC | 0.00289 | 0.85 | 0.96 | 0.78 | 0.98 | 0.46 | 0.20 | 0.71 |
| W_NMS | 0.00169 | 0.93 | 0.94 | 0.92 | 0.98 | 0.84 | 0.66 | 0.88 |
| W_MLC | 0.00183 | 0.81 | 0.96 | 0.91 | 0.99 | 0.68 | 0.49 | 0.81 |

234 **Table S1.** Comparative performance of the NMS, W_NMS, MLC and W_MLC calibrations based
 235 on the independent WD-XRF evaluation dataset.

236

| | XRF core-scanning | | | WD-XRF | | |
|--------------------------------|---------------------------|---------------------------|---------------------------|----------------------------|---------------------------|---------------------------|
| | <i>a</i> | <i>b</i> | <i>c</i> | <i>a'</i> | <i>b'</i> | <i>c'</i> |
| NPS | | | | | | |
| Al ₂ O ₃ | -1.80469×10 ⁻⁴ | 1.68432×10 ⁰ | 8.97978×10 ³ | 2.78273×10 ⁻⁹ | -8.40326×10 ⁻⁵ | 1.37066×10 ¹ |
| SiO ₂ | -2.45332×10 ⁻³ | 1.79966×10 ¹ | 1.00061×10 ⁵ | -1.81234×10 ⁻⁷ | 2.41132×10 ⁻⁴ | 4.51526×10 ¹ |
| K ₂ O | -1.41146×10 ⁻³ | 1.02346×10 ¹ | 7.65880×10 ⁴ | -1.51777×10 ⁻⁸ | 7.41048×10 ⁻⁵ | 2.50604×10 ⁰ |
| CaCO ₃ | 7.41644×10 ⁻³ | 1.63646×10 ¹ | 3.49452×10 ⁵ | 7.16093×10 ⁻⁸ | 1.12871×10 ⁻³ | 1.62933×10 ¹ |
| TiO ₂ | -3.86774×10 ⁻⁴ | 2.12999×10 ⁰ | 2.59334×10 ⁴ | -1.23080×10 ⁻⁹ | 1.69629×10 ⁻⁶ | 3.50704×10 ⁻¹ |
| Fe ₂ O ₃ | -2.86182×10 ⁻³ | 1.37946×10 ¹ | 2.67617×10 ⁵ | 9.82231×10 ⁻⁹ | -4.98498×10 ⁻⁵ | 5.19958×10 ⁰ |
| P_MLC | | | | | | |
| Ln(Al/Ca) | -3.02644×10 ⁻⁸ | 1.05644×10 ⁻⁴ | -3.62151×10 ⁰ | -1.09977×10 ⁻⁹ | -7.01019×10 ⁻⁵ | 1.22727×10 ⁻¹ |
| Ln(Si/Ca) | -3.34144×10 ⁻⁸ | 9.94519×10 ⁻⁵ | -1.20827×10 ⁰ | -5.30853×10 ⁻⁹ | -5.91265×10 ⁻⁵ | 1.18852×10 ⁰ |
| Ln(K/Ca) | -2.84439×10 ⁻⁸ | 6.29718×10 ⁻⁵ | -1.47834×10 ⁰ | -7.18546×10 ⁻⁹ | -3.55063×10 ⁻⁵ | -1.12705×10 ⁰ |
| Ln(Ti/Ca) | -2.62373×10 ⁻⁸ | 2.14666×10 ⁻⁵ | -2.56272×10 ⁰ | -3.60930×10 ⁻⁹ | -6.01153×10 ⁻⁵ | -2.90324×10 ⁰ |
| Ln(Fe/Ca) | -2.23219×10 ⁻⁸ | -7.08975×10 ⁻⁶ | -2.29677×10 ⁻¹ | -4.20260×10 ⁻¹⁰ | -7.35452×10 ⁻⁵ | -5.66757×10 ⁻¹ |

237 **Table S2.** Parameters of quadratic polynomial equations applied to XRF-scan element intensities
 238 and WD-XRF component concentrations in NPS calibration (equations S4), as well as XRF-scan
 239 and WD-XRF element log-ratios in P_MLC calibration (equation S6).

- 240 **Data Set S1.** Discrete measurements of core MD12-3432. WD-XRF data (both calibration and
241 evaluation dataset), dry bulk density and water content are included.
- 242 **Data Set S2.** XRF core scanning data of core MD12-3432 used in the calibration.
- 243 **Data Set S3.** ICP-AES data of core MD12-3432 used to verify the accuracy of WD-XRF analyses.