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## Corrigenda of 'Explicit wave-averaged primitive equations using a Generalized Lagrangian Mean'

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### Abstract :

Ardhuin et al. (2008) gave a second-order approximation in the wave slope of the exact Generalized Lagrangian Mean (GLM) equations derived by Andrews and McIntyre (1978), and also performed a coordinate transformation, going from a from GLM to a 'GLMz' set of equations. That latter step removed the wandering of the GLM mean sea level away from the Eulerian-mean sea level, making the GLMz flow non-divergent. That step contained some inaccurate statements about the coordinate transformation, while the rest of the paper contained an error on the surface dynamic boundary condition for viscous stresses. I am thankful to Mathias Delpey and Hidenori Aiki for pointing out these errors, which are corrected below.

## 11 **1 Surface boundary condition and virtual wave stress**

12 In their equation (61) Ardhuin et al. (2008) wrongly separated the average  
13 stress as a horizontal force and a vertical force acting on the surface. Instead,  
14 it is more appropriate to follow the many investigations on the subject and to  
15 separate the stresses as a normal and a tangential stress (e.g. Jenkins, 1992).  
16 The horizontal component of the normal stress is the usual pressure-slope  
17 correlation that we will denote  $\tau_w$ , and which is often called 'wave-supported

18 stress' which is slightly incorrect given the other (small) part of the wave-  
 19 supported stress that is the oscillatory shear stress. The interesting part here,  
 20 and the source of error in the paper is the tangential stress, which is along the  
 21 surface has a local value given by Longuet-Higgins (1953), and also discussed  
 22 in Xu and Bowen (1994), among others. Here we use the expression given by  
 23 Dore (1970, eq. 3.18), valid at the instantaneous sea surface  $z = \zeta$

$$24 \quad \tau_t = \mu \left[ \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} - 4 \frac{\partial \zeta}{\partial x} \frac{\partial u}{\partial x} \right]. \quad (1)$$

25 As stated by Dore (1970), the proper boundary condition is thus given by the  
 26 continuity of both the normal stresses and tangential stresses. In the case of  
 27 the GLM equations, the boundary condition for the tangential stress is thus  
 28 the horizontal projection of the GLM of eq. (2).

$$29 \quad \overline{\tau}_t^L = \mu \left[ \overline{\frac{\partial u}{\partial z} + \frac{\partial w^L}{\partial x}} - 4 \overline{\frac{\partial \zeta}{\partial x} \frac{\partial u^L}{\partial x}} \right]. \quad (2)$$

30 This tangential stress is clearly of second order in the wave slope  $ka$ , and thus  
 31 its projection on the horizontal only gives third or higher order correction. For  
 32 the purpose of averaging, we can thus consider this stress to be horizontal.

33 For the case of a zero quasi-Eulerian current, the first of these two terms was  
 34 already evaluated by Ardhuin and Jenkins (2006) using linear wave theory,  
 35 which is sufficient here given the small deviation caused by viscosity (e.g.  
 36 Dore, 1970, 1978). We thus only need to add the quasi-Eulerian mean current  
 37  $\hat{u}$  in the average, namely

$$38 \quad \overline{\frac{\partial u}{\partial z} + \frac{\partial w^L}{\partial x}} = \frac{\partial(U_s + \hat{u})}{\partial z} \quad (3)$$

39 with  $U_s$  the Stokes drift velocity, which, for monochromatic waves of amplitude  
 40  $a$ , radian frequency  $\sigma$  and wavenumber  $k$  is given by

$$41 \quad U_s = \sigma k \frac{a^2 \cosh(2kz + 2kh)}{2 \sinh^2(kD)}. \quad (4)$$

42 In the second term, due to the product of the surface slope and velocity gradi-  
 43 ent, which are each first-order terms in the wave slope  $ka$ , it is enough to use  
 44 an Eulerian approximation to the Lagrangian average, based on velocities in  
 45 the water, extrapolated to the mean sea surface at  $\zeta = 0$ . A rigorous Taylor  
 46 expansion up to  $\zeta = 0$  yields extra term which are at least of order  $(ka)^2$  for  
 47 the velocity gradient, and thus  $(ka)^3$  when multiplied by the slope. This has  
 48 already been evaluated by e.g. (Xu and Bowen, 1994, eq. 48),

$$49 \quad \overline{\frac{\partial \zeta}{\partial x} \frac{\partial u}{\partial x}} = \frac{\partial U_s}{\partial z}. \quad (5)$$

50 Hence the two terms of  $\tau_t$  that contain  $\partial U_s / \partial z$  cancel, leaving  $\partial \hat{u} / \partial z = 0$  at  
 51 this order, on  $z = \bar{\zeta}$ .

52 We thus obtain the mean continuity equation across the air-sea boundary in  
 53 which the wind stress  $\tau$  is the sum of the mean tangential and wave-supported  
 54 stresses right at the sea surface

$$55 \quad \tau = \overline{\tau^L} = \mu \frac{\partial \hat{u}}{\partial z} + \tau_w \quad \text{at} \quad z = \bar{\zeta}. \quad (6)$$

56 We note, however, that the subsurface shear, at a small distance  $\delta$  from the  
 57 free surface is increased by the momentum lost by waves associated to wave  
 58 dissipation. Indeed, in the absence of wind,  $\tau = \tau_w = 0$  and  $\partial \hat{u} / \partial z = 0$  right  
 59 at the surface. But this shear increases away from the surface, as measured  
 60 in the laboratory by Longuet-Higgins (1970), who found, at the base of the

61 viscous layer,  $\partial\hat{u}/\partial z = \partial U_s/\partial z$ . Indeed, the glm2z momentum equations (eq.  
 62 (42) in Arduin et al., 2008) can be integrated from  $z = \bar{\zeta}$  down to  $z = \bar{\zeta} - \delta$ ,  
 63 provided that the force  $\widehat{X}_\alpha$  is understood to represent all the momentum lost  
 64 by the wave field, including viscous dissipation. In the absence of wind, and  
 65 for constant wave conditions we have,

$$66 \quad \mu \frac{\partial \hat{u}}{\partial z} \Big|_{z=\bar{\zeta}-\delta} = - \int_{\bar{\zeta}-\delta}^{\bar{\zeta}} \widehat{X} dz. \quad (7)$$

67 For viscous dissipation, the momentum  $X$  lost by the wave field per unit  
 68 volume is concentrated near the surface, and its integral is the rate of loss of  
 69 wave energy divided by the phase speed, i.e.

$$70 \quad \int_{\bar{\zeta}-\delta}^{\bar{\zeta}} \widehat{X} dz = 2\mu g k^2 a^2 / (\sigma/k) = \mu \frac{\partial U_s}{\partial z}, \quad (8)$$

71 where the first equality is only valid for monochromatic waves in the  $x$  direc-  
 72 tion, while the second equality holds for a random sea state.

## 73 2 Vertical coordinate transformation from GLM to GLMz

74 In the transformation of the vertical coordinate Arduin et al. (2008) incor-  
 75 rectly defined the new coordinate by their eq. (48),

$$76 \quad s = z^* + \bar{\xi}_3^L \quad (9)$$

77 That transformation does not satisfy the desired equation (46) because of the  
 78 vertical stretching of  $\xi_3$ . Instead one may introduce a vertical displacement  $\zeta_c$

79 attached to a constant vertical coordinate  $c$ ,

$$80 \quad \zeta_c = \xi_3(x_\alpha, z = c, t). \quad (10)$$

81 As a result the Stokes correction of  $\zeta_c$ , just like for the position of the free  
82 surface, will only contain terms associated with horizontal gradients,

$$83 \quad \overline{\zeta_c^S} = \overline{\partial \frac{\zeta_c}{x_\alpha} \xi_\alpha|_{z=c}} + O(k^{-1}\epsilon^3) = \overline{\partial \frac{(\xi_3|_{z=c})}{x_\alpha} \xi_\alpha|_{z=c}} + O(k^{-1}\epsilon^3). \quad (11)$$

84 Using linear wave theory this gives

$$85 \quad \overline{\zeta_c^S} = \overline{(-ak_\alpha m F_{SS} \sin \psi) \times \left( -am \left[ \frac{k_\alpha}{k} F_{CS} + \frac{m}{\sigma} \frac{\partial \bar{u}_\alpha}{\partial z} F_{SS} \right] \sin \psi \right)} + O(k^{-1}\epsilon^3), \quad (12)$$

86 where  $\psi$  is the phase of waves and all notations are defined in Arduin et al.  
87 (2008).

88 Neglecting the effect of current shear,  $m = 1$ ,  $\partial \bar{u}_\alpha / \partial z = 0$

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$$\overline{\zeta_c^S} = \frac{1}{2} a^2 k (F_{CS} F_{SS})_{z=c} + O(k^{-1}\epsilon^3). \quad (13)$$

90 and we finally have the desired relation

$$91 \quad \frac{\partial}{\partial z} (\overline{\zeta_c^S}) = \frac{1}{2} a^2 k^2 (F_{CS}^2 + F_{SS}^2) + O(\epsilon^3) = J_2. \quad (14)$$

92 We may thus define implicitly the vertical coordinate  $z^*$  for each  $z = c$ ,

$$93 \quad z = s(z^*) = z^* + \overline{\zeta_c^S} \quad (15)$$

94 to obtain a non-divergent set of equations, and, in particular, a mean sea level  
95 that is at the Eulerian mean sea level.

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