Supporting Information for 1 "Fluctuations of the Atlantic North Equatorial Undercurrent and associated changes in oxygen transports"

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Introduction 12

In section S1 of the Supporting Information we give an detailed overview about the pro-13 cessing of the moored and shipboard observations. Section S2 presents details of the 14 estimation of eastward transports from zonal velocity observations, their accuracies and 15 uncertainties as well as their associated spatial patterns. In section S3 we investigate the 16 relation between the NEUC transport and zonal wind stress in the tropical Atlantic. 17

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¹⁸ S1: Moored and shipboard observations

¹⁹ Moored data

For our analysis we used velocity, hydrography and oxygen data from moorings at 20 5°N/23°W (Jul 2006-Feb 2008, Nov 2009-Jan 2018), 4.6°N/23.4°W (Nov 2012-Apr 2014) 21 and $4.5^{\circ}N/22.4^{\circ}W$ (Nov 2012-Apr 2014). At all three mooring positions horizontal ve-22 locity was measured with downward (Jul 2006-Feb 2008) or upward (Nov 2009-Jan 2018) 23 looking 75-kHz Longranger Acoustic Doppler Current Profilers (ADCPs). The ADCP 24 configuration was set to a sampling period of 2h, a bin length of 16 m and an ensemble 25 number of 20 pings. A single velocity data point has a standard error of $1.7 \,\mathrm{cm \, s^{-1}}$. Given 26 the manufacturer's compass accuracy of 2° , we inferred a velocity error of < 4 % of the 27 absolute measured velocity (Hahn et al., 2014). The minimum measurement range of all 28 mooring periods is 85 m to 755 m. The moored velocity data was linearly interpolated 29 onto a regular time-depth grid $(12 \text{ h} \times 10 \text{ m})$, and a 40-h low-pass Butterworth filter was 30 applied to remove the tidal signal from the time series (Fig. S1). 31

Eight pairs of oxygen (AADI Aanderaa optodes of model types 3830 and 4330) and 32 Conductivity-Temperature-Depth (CTD) sensors (Sea-Bird SBE37 microcats) were in-33 stalled at the moorings evenly distributed in the depth range from 100 m to 800 m. This 34 configuration allows an appropriate estimate of the dissolved oxygen on density surfaces. 35 All instruments were set to a sampling period of 2 h or shorter. The oxygen and CTD 36 sensors were calibrated against CTD casts performed directly prior to or after the de-37 ployment period of the mooring. The oxygen sensors were additionally calibrated against 38 laboratory measurements to expand the range of reference calibration points. For more 39 details of the oxygen calibration see Hahn et al. (2014). The root mean square error 40

of moored temperature, salinity and dissolved oxygen measurements was about 0.003° C, 0.006 and $3 \,\mu$ mol kg⁻¹, respectively (see Hahn et al., 2017). The point measured hydrography and oxygen data was interpolated onto a 12-h time grid.

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45 Shipboard data

⁴⁶ 24 meridional velocity and 15 hydrographic and oxygen sections between 21°W and 26°W
⁴⁷ were obtained during cruises between 2002 to 2018 (Table S1). All ship sections cover
⁴⁸ at least the upper 350 m between 0° and 10°N. The velocity, hydrographic and oxygen
⁴⁹ ship sections used in this study are an extension of the data set used in Burmeister et al.
⁵⁰ (2019).

Velocity data were acquired by vessel-mounted ADCPs (vm-ADCPs). Vm-ADCPs con-51 tinuously record velocities throughout a ship section and the accuracy of 1-h averaged data 52 is better than $2-4 \,\mathrm{cm \, s^{-1}}$ (Fischer et al., 2003). Hydrographic and oxygen data obtained 53 during CTD casts were typically performed on a uniform latitude grid with half-degree 54 resolution. The data accuracy for a single research cruise is generally assumed to be 55 better than 0.002°C, 0.002 and $2 \,\mu \text{mol kg}^{-1}$ for temperature, salinity, and dissolved oxygen, respectively (Hahn et al., 2017). The single velocity, hydrographic and oxygen ship 57 section were mapped on a regular grid $(0.05^{\circ} \text{ latitude} \times 10 \text{ m})$ and were smoothed by 58 a Gaussian filter (horizontal and vertical influence (cutoff) radii: 0.05° (0.1°) latitude 59 and 10 m (20 m), respectively). The single sections were averaged at each grid point to 60 derive mean sections, which are again smoothed by the Gaussian filter. For the mean ve-61 locity, temperature, salinity and oxygen sections the standard error in the NEUC region 62

 $_{63}$ (65 – 270 m depth, 3° – 6.5°N) are 1.7 cm s⁻¹, 0.22°C, 0.02 and 3.8 μ mol kg⁻¹, respectively.

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65 S2: NEUC transport calculations

66 Path following algorithm

⁶⁷ We derived estimates of the NEUC transport from the 24 meridional ship sections based ⁶⁸ on the algorithm of Hsin and Qiu (2012) which we consider as a reference NEUC transport. ⁶⁹ First, the central position Y_{CM} of the current is estimated using the concept of center of ⁷⁰ mass:

$$Y_{CM}(t) = \frac{\int_{Z_l}^{Z_u} \int_{Y_S}^{Y_N} y \ u(y, z, t) \ dy \ dz}{\int_{Z_l}^{Z_u} \int_{Y_S}^{Y_N} u(y, z, t) \ dy \ dz},\tag{1}$$

where y is latitude, u is zonal velocity, z is depth, t is time, Z_u (Z_l) is upper (lower) boundary of the flow, and $Y_N = 6^{\circ}N$ ($Y_S = 3.5^{\circ}N$) is the northern (southern) limit of the current core. We estimated a mean NEUC central position of 4.9°N and a standard deviation of $\pm 0.3^{\circ}$.

⁷⁵ Now the eastward velocity is integrated within a box whose meridional range is given ⁷⁶ by $Y_{CM}(t)$ and the southern (B_S) and northern (B_N) extent of the flow:

$$INT(t) = \int_{Z_l}^{Z_u} \int_{Y_{CM} - B_S}^{Y_{CM} + B_N} u(y, z, t) \, dy \, dz \tag{2}$$

For the integration we used the same boundary conditions as Burmeister et al. (2019). Z_u is the depth of the 24.5 kg m⁻³ and Z_l the depth of the 26.8 kg m⁻³ neutral density surface. The southern boundary is choosen as $Y_{CM} - 1.5^{\circ}$ and the northern boundary is $Y_{CM} + 1.0^{\circ}$. Note that, if no hydrographic measurements are available for a single ship

⁸¹ section, the neutral density field derived from the mean hydrographic section is used.

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Transport reconstruction

The eastward transport associated with the NEUC at about 23°W is computed using 84 moored velocity data at 5° N, 23° W (2006-2018) as well as 4.6° N, 22.4° W (Nov. 2012-85 Apr. 2014) and 4.5°N, 23.4°W (Nov. 2012-Apr. 2014) combined with 24 meridional 86 ship sections between 21°W and 26°W (Fig S1). In the main manuscript we reconstruct 87 the NEUC transport using the optimal width (OW) method as described in Brandt et 88 al. (2014). We chose this simple method because it is sufficient to represent the NEUC 80 variability and more complex methods do not add any value, which we will show in this 90 section. We validate the OW method using another approach from Brandt et al. (2014) 91 based on Hilbert empirical orthogonal functions (HEOFs). 92

In the second approach the meridional sections of zonal velocity are reconstructed from 93 the moored zonal velocities by interpolation and extrapolation using data taken at the 94 mooring position. For the reconstruction of meridional sections we use variability patterns 95 derived from the 24 meridional ship sections. Therefore we calculate HEOF pattern from the velocity sections between $4.25^{\circ}N$ and $5.25^{\circ}N$, 65 m and 270 m (black dashed frame in 97 Fig. S1). Here, a Hilbert transformation is applied to the zonal velocity fields before an 98 EOF analysis is performed. The advantage of an HEOF is that the statistical patterns 90 efficiently reveal spatial propagation features as for example a meridional migration of 100 the current, in contrast to a traditional EOF. The first HEOF pattern explains 56% of 101 variability contained in the ship section. The real pattern of the first HEOF shows a 102 homogeneous change of velocities over the complete integration area (Fig. S3). Using 103

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only the first HEOF patterns to interpolate between the mooring positions by regressing 104 the patterns onto the moored zonal velocity observations results in similar reconstructed 105 transports as the OW method (black and red line in Fig. S4). As the homogeneous 106 structure of the first HEOF explains most of the variability, there is no added value by 107 including more HEOF patterns to reconstruct the NEUC transport. Nevertheless we 108 want to mention here that the second pattern with a explained variance of 20% describes 109 a meridional shift of the NEUC. A vertical shift of the NEUC might be described by the 110 patterns of the third and fourth HEOF. 111

To investigate whether the dominant pattern of the first HEOF of the zonal velocities 112 between 4.25°N and 5.25°N represents a meridional migration of the NEUC out of the 113 calculation area the HEOF method is repeated using the zonal velocities between 3.5°N 114 and 6.0°N. This region covers the southern and northern boundary of the NEUC even if 115 the current is meridionally migrating. The fixed box integrated transports for this region 116 calculated from the ship sections (gray squares in Fig. S4) agrees well with the reference 117 transports. Again, the real pattern of the first HEOF shows a homogeneous change of 118 zonal velocity although it explains less variability compared to the first HEOF of the 119 smaller box. Furthermore, the first and second pattern which explain together 66% of the 120 velocity variability seem to describe a meridional shift of the current. Nevertheless, the 121 eastward transport time series reconstructed using the first (yellow line in Fig. S4) or the 122 first two HEOF pattern (blue line in Fig. S4) of zonal velocities between 3.5° N and 6.0° N 123 agrees well with that reconstructed from velocities between 4.25°N and 5.25°N. The mean 124 transport estimates using the bigger box is 1.9 Sv. 125

¹²⁶ In summary, the reconstructed eastward transports between 4.25°N and 5.25°N tend to ¹²⁷ underestimate the mean current strength of the NEUC, however the time series is able to ¹²⁸ capture the NEUC variability reasonably well. We choose the smaller box to reconstruct ¹²⁹ the NEUC transport variability due to the smaller uncertainty of the reconstructed trans-¹³⁰ ports when using only the mooring at 5°N, 23°W.

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¹³² S3: NEUC and sea surface winds

¹³³ Auxiliary data

¹³⁴ Monthly mean JRA-55 surface wind velocities (U_h , Kobayashi et al., 2015) on a ¹³⁵ $1.25^{\circ} \times 1.25^{\circ}$ horizontal grid for the time period from 2006 to 2018 are used in this study. ¹³⁶ We calculated the wind stress τ_h from the JRA-55 reanalysis data using the Bulk formula ¹³⁷ $\tau_h = \rho_{air} C_D |U_h| U_h$, where $\rho_{air} = 1.22 \text{kg m}^{-3}$ is the density of air, $C_D = 0.0013$ is the wind ¹³⁸ drag coefficient and $|U_h|$ is the absolute value of U_h .

Furthermore, we are using monthly mean wind stress from the ASCAT on METOP Level 4 Daily Gridded Mean Wind Fields (Bentamy & Fillon, 2012). The dataset has a horizontal resolution of 0.25° covering the time period from April 2007 to May 2018. For comparison, ASCAT wind stress data are regridded onto the horizontal grid of the JRA-55 reanalysis data (1.25°) by bin averaging.

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¹⁴⁵ Linear regression

¹⁴⁶ We performed a lead-lag regression of zonal wind stress anomalies with respect to the ¹⁴⁷ 2008 to 2017 climatology onto the reconstructed NEUC time series for two different wind ¹⁴⁸ products (Fig. S6). The regression pattern of both wind products generally agree. Differ-

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ences in the wind stress products may arise from the different kind of data that is used. Another source of uncertainty may be different Bulk formulas used for the wind stress calculations, which can result in an uncertainty up to 20% (Large & Yeager, 2004).

In the linear regression patterns, easterly wind stress anomalies between 12° S and 6° N 152 east of about 25°W are leading the NEUC transports by one to two months. Along the 153 equator, these easterly wind stress anomalies may trigger equatorial Kelvin waves. These 154 Kelvin waves may remotely generate Rossby waves traveling as far as 5°N, 23°W by 155 reflecting at the eastern boundary into Rossby waves and coastal trapped waves traveling 156 northward along the coast and generating Rossby waves when the topography is turning 157 north. Rossby waves at 5°N, 23°W may also be generated locally (Burmeister et al., 2016; 158 Foltz et al., 2010). In the ASCAT and JRA-55 data easterly wind stress anomalies above 159 the NEUC region with decreasing magnitude towards the north lead the NEUC transports 160 by two months. The decreasing zonal wind stress indicates changes in the wind stress 161 curl, which may locally generate Rossby waves altering the NEUC flow. Furthermore 162 local zonal wind stress anomalies along the northern coastline of the Gulf of Guinea can 163 trigger westward propagating coastal trapped waves which again generate Rossby waves 164 radiating from the coast when the topography turns north (Chu et al., 2007). In general, 165 the relative low coefficient of correlation (R < 0.45) suggest that the wind stress field can 166 only explain some part of the NEUC variability and other processes must contribute. 167

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Table S1. Meridional ship sections taken between 21° W and 26° W from 2002 to 2018. All sections cover at least the upper 350 m from 0° N to 10° N. For all sections ADCP data is available. Sections including oxygen (O₂) and hydrography (CTD) measurements are marked accordingly.

			averaged		
cruise		date	longitude	latitude	O_2/CTD
Meteor 55	Oct-Nov	2002	$24^{\circ}W$	0°-10°N	no
Ronald H. Brown A16N	Jun-Aug	2003	$26^{\circ}W$	$6^{\circ}\text{S-}10^{\circ}\text{N}$	no
Ronald H. Brown PNE6	Jun	2006	$23^{\circ}W$	$5^{\circ}\text{S-13.5}^{\circ}\text{N}$	yes
Ronald H. Brown PNE6	Jun-Jul	2006	$23^{\circ}W$	$5^{\circ}\text{S-}14^{\circ}\text{N}$	yes
Meteor $68/2$	Jun-Jul	2006	$23^{\circ}W$	$4^{\circ}\text{S-}14^{\circ}\text{N}$	yes
L'Atalante IFM-GEOMAR 4	Feb	2008	$23^{\circ}W$	$2^{\circ}\text{S-}14^{\circ}\text{N}$	yes
L'Atalante IFM-GEOMAR 4	Mar	2008	$23^{\circ}W$	$2^{\circ}\text{S-}14^{\circ}\text{N}$	no
Ronald H. Brown PNE09	Jul-Aug	2009	$23^{\circ}W$	0° - $14^{\circ}N$	no
Meteor $80/1$	Oct-Nov	2009	$23^{\circ}W$	$6^{\circ}\text{S-}14^{\circ}\text{N}$	yes
Meteor $81/1$	Feb-Mar	2010	$21^{\circ}W$	$6^{\circ}\text{S-}13^{\circ}\text{N}$	no
Ronald H. Brown PNE10	May	2010	$23^{\circ}W$	0° - $14^{\circ}N$	yes
Maria S. Merian $18/2$	May-Jun	2011	$23^{\circ}W$	0° - $14^{\circ}N$	no
Ronald H. Brown PNE11	Jul-Aug	2011	$23^{\circ}W$	0° - $14^{\circ}N$	no
Maria S. Merian 22	Oct-Nov	2012	$23^{\circ}W$	$6^{\circ}\text{S-}8^{\circ}\text{N}$	yes
Maria S. Merian 22	Oct-Nov	2012	$23^{\circ}W$	0° - $14^{\circ}N$	no
Ronald H. Brown PNE13a	Jan-Feb	2013	$23^{\circ}W$	0° - $14^{\circ}N$	no
Ronald H. Brown PNE13b	Nov-Dec	2013	$23^{\circ}W$	$6^{\circ}\text{S-}14^{\circ}\text{N}$	yes
Meteor 106	Apr-May	2014	$23^{\circ}W$	$6^{\circ}\text{S-}14^{\circ}\text{N}$	yes
Polarstern PS88.2	Oct-Nov	2014	$23^{\circ}W$	$2^{\circ}\text{S-}14^{\circ}\text{N}$	yes
Endeavor EN-550	Jan	2015	$23^{\circ}W$	$2^{\circ}\text{S-}14^{\circ}\text{N}$	yes
Meteor 119	Sep-Oct	2015	$23^{\circ}W$	$5.5^{\circ}\text{S-}14^{\circ}\text{N}$	yes
Meteor 130	Aug-Oct	2016	$23^{\circ}W$	$6^{\circ}\text{S-}14^{\circ}\text{N}$	yes
Ronald H. Brown PNE17	Feb-Mar	2017	$23^{\circ}W$	$4^{\circ}\text{S-}14^{\circ}\text{N}$	yes
Meteor 145	Feb-Mar	2018	$23^{\circ}W$	$6^{\circ}\text{S-14}^{\circ}\text{N}$	yes



Figure S1. (a) Mean zonal velocity along 23°W estimated on the basis of 24 ship sections taken during 2002 and 2018. Black vertical lines mark the latitudinal position of the three moorings. The black dashed frame marks the box for the transport reconstruction. (b,c,d) Zonal velocity observations at the mooring positions (b) 5.0°N, 23°W, (c) 4.6°N, 23.4°W and (d) 4.5°N, 22.4°W.



Figure S2. Regression slope b, mean difference D and correlation coefficient R between the reference NEUC transport (along-pathway transport) and the reconstructed transports based on different methods: (a) fixed box integrated transports between 4.25°N and 5.25°N (green) as well as between 3.50°N and 6.00°N (purple), (b) OW method using 3 moorings (red) and only the 5°N mooring, (c) HEOF method using the first HEOF pattern applied to 3 moorings (orange) and only to the 5°N mooring (yellow) for the area between 4.25°N and 5.25°N, (d) HEOF method using the first HEOF pattern applied to 3 mooring (grey) for the area between 3.50°N and 6.00°N.



Figure S3. Real (left panels) and imaginary (right panels) dimensionless pattern of the first four Hilbert empirical orthogonal functions calculated from the 24 zonal velocity sections along 23°W between 4.25°N and 5.25°N, 65 m and 270 m depth.



Figure S4. NEUC transport at 23°W calculated by different methods: (i) from ship observations using a path following algorithm (green diamonds); (ii) from ship sections by integrating the eastward velocities in a fixed box between 4.25°N and 5.25°N (black circles) and 3.5°N and 6.0°N (grey squares); (iii) by the HEOF method combining ship sections and moored zonal velocities at three mooring positions using the first HEOF of velocities between 4.25°N and 5.25°N (black line) as well as using the first (orange line) or the first two (blue line) HEOF of velocities between 3.5°N and 6.0°N; (iv) by the OW method combining ship sections between 4.25°N and 5.25°N and moored zonal velocities at three mooring positions (red line).



Figure S5. Real (left panels) and imaginary (right panels) dimensionless pattern of the first four Hilbert empirical orthogonal functions calculated from the 24 zonal velocity sections along 23°W between 3.5°N and 6.0°N, 65 m and 270 m depth.



Figure S6. Slope of lead-lag regression of monthly mean zonal wind stress anomalies with respect to the 2008-2017 climatology onto the reconstructed monthly mean NEUC transport time series. Results are shown for ASCAT (a-d) and JRA-55 reanalysis (e-h). Contour lines show the coefficient of correlation (R) with an interval of 0.1, the grey contour marks R=0.1. Grey crosses mark significant values of R.



Figure S7. 30-day low-pass filtered (a-c) meridional velocity anomalies (green lines) and oxygen anomalies (blue lines) at 5°N, 23°W at a depth of (a) 100 m, (b) 200 m, and (c) 300 m. Grey bars mark strong NEUC events. The correlation coefficient R at zero lag is not significant on a 95% confident interval.