# Science Advances

### Supplementary Materials for

## First source-to-sink monitoring shows dense head controls sediment flux and runout in turbidity currents

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#### **Supplementary Text**

Freshwater and sediment is delivered to the head of Bute Inlet by two rivers, the Homathko and Southgate Rivers. Of these, the Homathko supplies >80% of freshwater to Bute Inlet (*39, 40*). The deltas of these two rivers are incised by subaqueous channels which later merge, downstream of M6, to form a single channel which terminates about 43 km down-channel of the Homathko Delta (Fig. 1). As the confluence of the Homathko and Southgate branches of the channel occurs down-channel of M6, turbidity currents triggered on the Southgate Delta will not be identified in the ADCP records from M6. However, they may be identified at M4 if they runout sufficiently far. It is therefore important to identify a clear methodology for identifying where turbidity currents were most likely sourced.

Turbidity currents on the Homathko and Southgate Deltas are likely to be triggered under the same conditions due to their similar environmental setting (43). Both rivers drain mountainous glaciated catchments with peaks in river discharge associated with the Freshet which is a consequence of enhanced spring and summer glacier and snow melt (43). Previous studies of Bute Inlet turbidity currents, and flows in nearby Howe Sound, British Columbia, showed that flows were most likely triggered during periods when fluvial discharge was above a certain threshold and during periods when there was the greatest tidal range (39, 43, 53, 54). Nonetheless, turbidity currents sourced from the Homathko River are more likely given the greater sediment and freshwater supplied by this river (40).

Turbidity currents at M4 were therefore more likely to have been sourced from M6, when the arrival time at M4 was closely associated with arrival times of flows at M6. During the 206 day

deployment a total of 24 turbidity currents were observed at M4. Of these, the arrival times of 19 were associated with observed turbidity currents at M6. Using their arrival times, these flows had transit velocity of 0.3 to 4.8 m s<sup>-1</sup> over 8.5 km (Table s3).

Of the remaining five events, one (7/10/2018) is not associated with any turbidity current at M6 and is therefore thought to have originated from the Southgate Delta. The four other turbidity currents were judged to have originated from the Southgate Delta rather than the Homathko Delta. This is due to the extremely slow transit speeds ( $<0.05 \text{ m s}^{-1}$ ) at which they would need to travel, if they were remnants of the temporally closest event at M6. Moreover, the turbidity currentss with which they may have been associated with at M6 had slow ADCP-measured velocities at M6. This suggests that the flows were already weak at M6, making their passage as far as M4 unlikely.

In addition to these additional five distinct turbidity currents inferred to come from the Southgate Delta, an additional turbidity current appears to have arrived (07/08/2018 17:04:50) at M4 during the passage of another flow (arrived at 07/08/2018 11:30:14). The initial flow was observed at M6, and is therefore believed to have originated from the Homathko Delta; this initial flow took ~73 minutes to traverse the ~10 km between M6 and M4. A second flow was observed to have arrived at M6 soon after the passage of the first flow. If this second flow is the same as the second flow pulse observed in M4, then it traversed the ~10 km between moorings in ~62 minutes. However, this is unlikely as the peak measured velocities of the flow at M6 (<1 m s<sup>-1</sup>) and its other flow characteristics (see Tables 1 and s3) suggest that the flow was too slow moving and dilute to have reached M4 this quickly. We therefore believe that this secondary flow pulse was also sourced from the Southgate Delta.

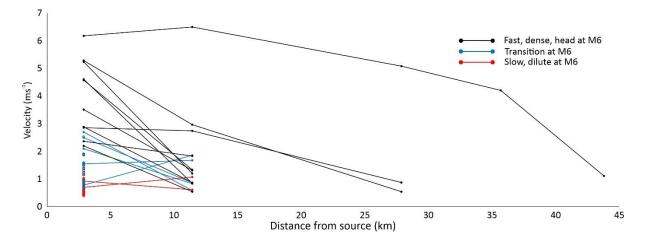


Fig. S1. Maximum measured velocities of turbidity currents in Bute Inlet relative to their structure type at M6.

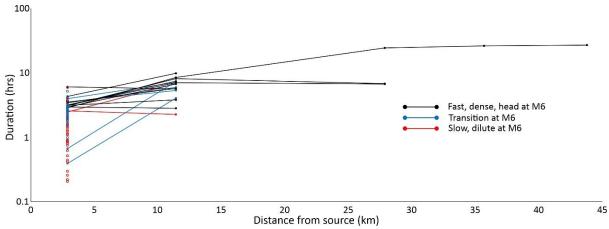


Fig. S2. Measured durations of turbidity currents in Bute Inlet relative to their structure type at M6.

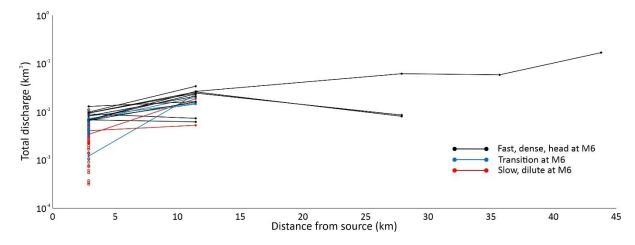


Fig. S3. Total discharge (sediment and water) of turbidity currents in Bute Inlet relative to their structure type at M6.

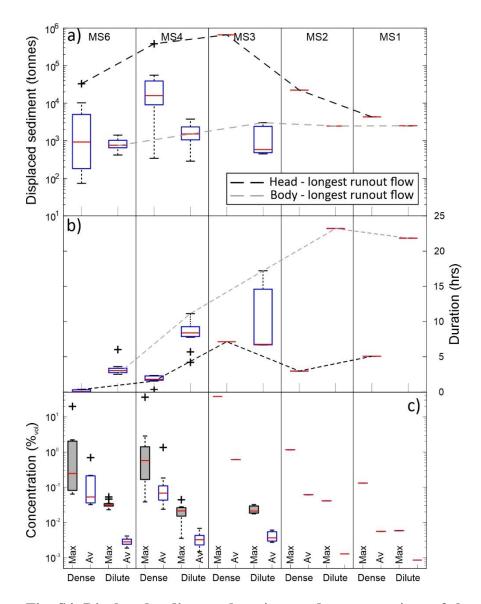


Fig. S4. Displaced sediment, durations and concentrations of the dense and dilute parts of turbidity currents in Bute Inlet characterised as having a fast, dense head at M6. The dense and dilute parts of the turbidity currents are defined by when  $C_{fb} > C_{fi}$  and when  $C_{fb} < C_{fi}$ . All calculations are based on iteratively solved Chézy equations assuming a bed friction coefficient ( $C_{fb}$ ) of 0.004.

		ADCP	Height		Temporal	Distance	Slope
		freqeuncy	above	Vertical bin	resolution	from delta	angle
Mooring	Depth (m)	(kHz)	bed (m)	size (m)	(seconds)	front (m)	(°)
MS6	176	300	30	1	(	6 2880	) 3.15
MS5	304	600	-	0.5		6 11420	4.36
MS4	314	600	25	0.5	(	6 12080	) 1.15
MS3	472	300	~8	0.5	(	6 27870	0.97
MS2	562	600	20	1	(	6 35690	) 1.59
MS1	607	600	20	1		4 43800	0.16

 Table S1. Specifications and location information for the moorings and instruments used in this study.

# Table S2. Dates of turbidity currents originating from the Homathko Delta and measuredbackground velocities before the arrival of the observed flows.

	Mooring M6		Maorin	ng M4	Moori	ng M3	Mooring M2	Mooring M1
		Background	1	Background		Background	Background	Background
		velocity		velocity		velocity	velocity	velocity
Flow Number		(m/s)	Date	(m/s)	Date	(m/s)	Date (m/s)	Date (m/s)
	14/05/2018 16/05/2018	0.117						
3	22/05/2018	0.100						
	22/05/2018 26/05/2018	0.096						
	27/05/2018	0.097						
7	28/05/2018		28/05/2018	0.047	29/05/2018	0.117		
	12/06/2018 20/06/2018	0.109						
	20/06/2018	0.098						
	21/06/2018	0.097						
	21/06/2018 22/06/2018	0.099	21/06/2018	0.055				
	22/06/2018	0.099						
	22/06/2018	0.096						
	23/06/2018 23/06/2018	0.094						
	24/06/2018	0.092						
19	25/06/2018	0.097						
	26/06/2018	0.102						
	30/06/2018 04/07/2018	0.091	05/07/2018	0.043				
	05/07/2018	0.100						
	07/07/2018	0.099						
	08/07/2018 08/07/2018	0.092						
27	08/07/2018	0.093						
	08/07/2018	0.105						
	09/07/2018 10/07/2018	0.086						
31	10/07/2018	0.081	10/07/2018	0.047				
	11/07/2018	0.093	11/07/2010	0.000				
	11/07/2018	0.083	11/07/2018	0.060				
	12/07/2018		12/07/2018	0.062				
	13/07/2018	0.095						
	21/08/2018 22/07/2018	0.089						
39	22/07/2018	0.090	22/07/2018	0.036				
	23/07/2018	0.093						
	24/07/2018 24/07/2018	0.098	24/07/2018	0.040				
43	25/07/2018	0.104						
	25/07/2018 26/07/2018	0.082						
	27/07/2018	0.088						
47	27/07/2018	0.085						
	29/07/2018	0.091	29/07/2018	0.043				
	31/07/2018 31/07/2018	0.098						
	01/08/2018	0.094						
	01/08/2018	0.098						
	01/08/2018 01/08/2018	0.099						
55	01/08/2018	0.092	02/08/2018	0.048				
	03/08/2018	0.101						
	04/08/2018 05/08/2018	0.099 0.098						
59	05/08/2018	0.089						
	05/08/2018	0.096	05 (00 (0010		00 (00 (0010	0.105		
	06/08/2018 06/08/2018	0.102	06/08/2018	0.042	06/08/2018	0.106		
63	06/08/2018	0.087						
	06/08/2018 07/08/2018	0.100	07/08/2012	0.047				
	07/08/2018	0.097	07/08/2018 07/08/2018	0.047 N/A				
67	08/08/2018	0.102						
	08/08/2018	0.093						
	09/08/2018	0.096						
71	10/08/2018	0.102						
	10/08/2018	0.083	10/08/2018	0.049				
	11/08/2018 11/08/2018	0.092 0.087						
	15/08/2018	0.088						
	16/08/2018	0.102						
	16/08/2018 19/08/2018	0.085	19/08/2018	0.035				
79	20/08/2018	0.091	20/08/2018		20/08/2018	0.099	20/08/2018 0.059	20/08/2018 0.049
	21/08/2018	0.096						
	21/08/2018 21/08/2018	0.083						
	23/08/2018	0.094						
84	24/08/2018	0.089						
	27/08/2018	0.087						
	30/08/2018 01/09/2018	0.096						
88	01/09/2018	0.087	01/09/2018	0.047				
	04/09/2018	0.088						
	05/09/2018 05/09/2018	0.087						
	06/09/2018	0.082						
	07/09/2018	0.087						
94	08/09/2018 11/09/2018	0.081 0.091						i l

					Sediment													Sediment							ediment						Sediment
	Maximum ADCP			Maximum sediment			Maximum ADCP			Maximum S sediment v			ADCP	m			laximum ediment			Maxim				taximum v ediment d			Maximun ADCP	с.	Water volume	Maximum sediment	volume displaced
M5 Flows Flow Typ	velocity	Duration I	Displaced	discharge	(metric M4	Flow Type	velocity I		Displaced	discharge d	isplaced N	13 lows Flow Ty	velocity		ation Dis irs) (kn	placed d	ischarge	(metric	M2	velocit w Type (m/s)	ty Duri	tion Dis	placed d	ischarge (i sg/s) b	netric	M1 Flows Flow Typ	velocity	Duration (hours)	Displaced (km3)	discharge	(metric tons)
1 Type 2	1.58	2.06	0.0058	75	141	тном тур	e (m/sj	nours	(kma)	(kg/s) (1	9 6	lows How I	/pe (m/s)	(nou	irs) (kri	na) (a	(2/3)	tonsj	FIOWS FIO	wiype (m/s)	luor	rs) (kr	13) (	(g/s) 0	ansy	FIGWS FIGW Typ	e (m/s)	(nours)	(kms)	(kg/s)	tonsj
2 Type 3 3 Type 2	0.94	2.60	0.0036	29 119																											
4 Type 2 5 Type 3	0.94	2.07	0.0044 0.0044	6 35																											
6 Type 3	0.56	0.22	0.0003	8	1																										
7 Type 1 8 Type 2	2.85	1.65	0.0094	8	1,538 27	Type 1	2.74	10.52	0.0243	12,664	57,027	Type	3 0	.87	6.69	0.0085	387	448													
9 Type 3 10 Type 2	0.48	1.57 2.18	0.0022	2 30	2 87																										
11 Type 3	0.45	0.30	0.0005	5	1																										
12 Type 1 13 Type 3	2.88	0.84	0.0090	6	1,830 2	Type 3	0.86	4.22	0.0073	15	302																				
14 Type 3 15 Type 3	0.65	1.56 2.82	0.0025	3	3 37																										
16 Type 3	0.65	2.26	0.0040	3	12																										
17 Type 2 18 Type 1	1.86	2.94	0.0086	452	486	Type 1	1.82	10.03	0.0233	2,192	24,384																				
19 Type 3 20 Type 3	0.66		0.0055	9	21 23																										
21 Type 2	2.45	3.53	0.0081	201	555	Type 2	0.86	7.97	0.0149		1,734																				
22 Type 2 23 Type 3	2.65	1.61	0.0010	8	5	Type 3	0.57	6.07	0.0104	16	423																				
24 Type 2 25 Type 2	1.15	2.74	0.0057	16 73	47																										
26 Type 3	1.31	3.35	0.0073	19	71																										
27 Type 3 28 Type 3	1.15	1.22	0.0053	6	52																										
29 Type 3 30 Type 3	0.85	2.86	0.0054	11	6 35 10 12																										
31 Type 3	0.92	2.57	0.0040	6	12	Type 3	0.61	3.39	0.0052	22	175																				
32 Type 3 33 Type 2	0.86	0.67	0.0042	14	10	Type 1	1.85	10.98	0.0229	1,633	14,137																				
34 Type 1 35 Type 1	1.88	3.61	0.0067	209	643	Type 2	1.33	11.11	0.0209		10,479																				
36 Type 3	0.68	1.96	0.0035	12	15																										
37 Type 3 38 Type 2	0.83	2.01	0.0036	81	14 195																										
39 Type 1 40 Type 2	4.65		0.0094			Type 2	1.46	10.05	0.0200	1,065	11,479																				
41 Type 3	0.74	1.29	0.0020	4	4																										
42 Type 2 43 Type 3	2.05	1.10	0.0072 0.0023	5	131 15	Type 2	0.82	8.94	0.0144	163	1,580																				
44 Type 2 45 Type 3	1.53		0.0063	181	344																										
46 Type 3	0.58	0.91	0.0017	19	6																										
47 Type 2 48 Type 1	0.64	6.05	0.0042 0.0128	6,401	12 1,485	Type 2	0.83	8.45	0.0162	180	3,764																				
49 Type 3 50 Type 2	0.57		0.0047	8	20																										
51 Type 3	0.43	0.41	0.0007	2	1																										
52 Type 3 53 Type 3	1.01	2.81	0.0052	19	25																										
54 Type 3 55 Type 1	0.61		0.0023	4 923		Type 2	1.30	8.59	0.0160	195	2,744																				
56 Type 3	1.40	3.98	0.0067	21																											
58 Type 3	0.43	2.01	0.0030	5	2																										
59 Type 3 60 Type 2	0.54		0.0025	4	4 662																										
61 Type 1	5.28	3.07	0.0094	2,178		Type 1	2.96	12.17	0.0257	3,108	22,773	Type	3 0	.53	6.78	0.0080	613	583													
63 Type 2	1.48	2.42	0.0044	88	174																										
64 Type 2 65 Type 2	0.84		0.0038	13 3,446	1,183	Type 2	1.19	14.73	0.0337	294	158																				
66 Type 2 67 Type 3	0.92	2.54	0.0045	21 35	27 48																										
68 Type 2	1.58	2.47	0.0063	155	491																										
69 Type 2 70 Type 2	1.51	2.40	0.0066	19	195																										
71 Type 3 72 Type 2	0.70	2.16	0.0040	10 84	28	Type 2	1.67	10.67	0.0198	1,187	10,843																				
73 Type 3	0.77	0.21	0.0003	1	0	. Here's	2.07	10.01	0.0120		10,0-3																				
74 Type 3 75 Type 3	1.30	2.57	0.0068	19 15	13																										
76 Type 3 77 Type 3	1.00	2.03	0.0041	13 2	37 15																										
78 Type 2	0.65	2.46	0.0034	12	11	Type 2	1.07	10.20	0.0185		91																				
79 Type 1 80 Type 3	6.13 0.52	1.12	0.0068	2	4	Type 1	6.49	12.70	0.0263	369,318	381,851	Туре	1 5	.08	24.35	0.0614	276,015	663,095		ype 1	4.20	26.18	0.0582	12,734	24,792	Type 2	1.1	1 26.9	1 0.167	9 80	4 6,81
81 Type 2 82 Type 3	2.52	3.09	0.0061	245 2	453 0																										
83 Type 3	0.55	0.44	0.0006	1	0	Acres 1			0.0017																						
84 Type 2 85 Type 3	0.72	0.89	0.0047	23 9	32 3	Type 3	0.71	1.64	0.0017	23	94																				
86 Type 3 87 Type 2	0.66		0.0009	2	1 23																										
88 Type 1	2.15	3.13	0.0068	356		Type 3	0.53	5.70	0.0062	97	286																				
89 Type 3 90 Type 3	0.38	1.48	0.0011 0.0030	12 22	2 33 27																										
91 Type 3 92 Type 3	0.95	5.92	0.0106	6	27																										
93 Type 3	0.65	1.84	0.0030	37	12 20																										
94 Type 3 95 Type 3	0.50	1.79	0.0026	4	23 12																										
Mean All Flow Mean Type 1	s 1.33 3.72	2.27	0.0046	2,064	690 Mean		1.56 3.17	8.85 11.28	0.0172		28,549 N	tean All Flo tean Type			12.60 24.35	0.0260		221,375	Mean Al	I Flows	4.20	26.18	0.0582	12,734	24,792	Mean All Flow	1.1	1 26.9	0.167	9 80	6,81
Mean Type 2	1.51	2.59	0.005	646 26	214 Mean	Type 2	1.17	10.08	0.019		4,763 N 256 N	tean Type	2	.70	6.73	0.008	500	516													
Mean Type 3	0.75	1.89	0.003	26	26 Mean	Type 3	0.66	4.20	0.008		250 1	tean Type	. 0	10	0.75	0.008	500	516													

### Table S3. Summary of turbidity current properties from the 2018 deployment in Bute Inlet.

			Maximum ADCP Velocity	Duration	Water volume displaced	Maximum sediment discharge	Sediment volume displaced		
Flow	Date	Time	(m/s)	(hours)	(km3)	(kg/s)	(tonnes)		
1	05/07/2018	17:47:02	0.639	8.09	0.00450	63	301.45		
2	15/07/2018	19:09:24	0.38	4.91	0.00000	134	0.56		
3	17/07/2018	20:29:02	0.391	7.78	0.00005	40	316.10		
4	07/08/2018	17:04:50	1.117	9.15	0.00500	498	4584.48		
5	26/08/2018	22:24:38	0.4223	2.43	0.00010	59	67.17		
6	07/10/2018	01:10:56	0.422	6.97	0.00212	47	221.49		

Table S4. Turbidity current characteristics of flows observed at M4 believed to haveoriginated from the Southgate Delta.